

# Probability and Statistics Notes

## Note 8

### Classical Upper Confidence Limits for the Failure Probability of Systems

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#### Abstract

The compute code CONLIM evaluates classical upper confidence limits for failure probability of systems based on component test results. CONLIM can accommodate systems ranging from the very simple to complex combinations utilizing several different components. Required input basically consists of component test data (number tested and number of failures) and the system reliability equation. This report (1) details the analysis for maximization of the nonlinear reliability function of many variables subject to a nonlinear constraint function, (2) develops the algorithms used in CONLIM, (3) provides a users' manual for the program, and (4) presents program output and computation times for several hypothetical systems demonstrating the flexibility of the code.

Key Words: Probability, confidence limits, nonlinear function maximization, hypervolumes, mathematical analysis, computer program

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## CLASSICAL UPPER CONFIDENCE LIMITS FOR THE FAILURE PROBABILITY OF SYSTEMS

### I. Introduction

Most functional systems represent a combination of many different components or elements. The systems might be electrical, mechanical, or in general, any assemblage of small units which makes up a larger unit. We are concerned with determining a classical upper confidence limit for the probability of failure of such systems from test information about the components. To accomplish this task, we divide the problem into three major parts: (1) the construction of a set of "hypervolumes" to be used in repeated computations to evaluate a constraint equation, (2) the maximization of a nonlinear function of many variables subject to a constraint, and (3) the development of an algorithm to place the theory into application.

In this report we discuss in detail each of these parts of the problem, as well as provide an extensive set of appendices covering the use of a computer program CONLIM. Included in the appendices are summarized tabulations of results obtained from sample test cases, a listing of the program CONLIM, sample input data formats and computer output reports, and an explanation of the variety of options available to the user of CONLIM.

## II. Basic Equations and Notation

Throughout this report several fundamental notations will be used which pertain to a system under study and each of the system components.

These notations are

- $n$  = number of unique system components;
- $m_i$  = number of performance tests on component  $i$ ,  $i=1, \dots, n$ ;
- $x_i$  = number of failures occurring in the tests of component  $i$ ,  $i=1, \dots, n$ ;
- $\alpha$  = confidence level at which the upper limit of system failure probability is to be computed.

(II-1)

The value of  $n$  is also defined to be the dimension of the system under consideration.

As described by Steck [1], the classical upper confidence limit on system failure probability is the maximum of the system failure probability function  $f(p_1, p_2, \dots, p_n)$  where  $p_i$  is the failure probability of the  $i$ th component in the system, subject to a constraint. Thus, we wish to find the values of the independent variables  $(p_1^*, p_2^*, \dots, p_n^*) = P^*$  such that  $f(P^*)$  is the maximum function value attainable subject to the constraint that

$$H(p_1^*, p_2^*, \dots, p_n^*) = 1 - \alpha \quad (\text{II-2})$$

where

$$H(p_1, p_2, \dots, p_n) = \sum_{a \in \Psi} \prod_{i=1}^n \binom{m_i}{a_i} p_i^{a_i} (1-p_i)^{m_i-a_i} \quad (\text{II-3})$$

and  $\Psi$  is an appropriately defined index set of vectors  $A = (a_1, a_2, \dots, a_n)$ . Adopting a proposal of Müller for specifying a reasonable set  $\Psi$  while avoiding the iterative computations required by Steck, we define the index set  $\Psi$  as all vectors  $A$  so that  $f(\bar{A}) \leq f(\bar{P})$  where

$$\bar{A} = (\bar{a}_1, \dots, \bar{a}_n) ; \bar{a}_i = \frac{a_i + 1}{m_i + 2} ; 0 \leq a_i \leq m_i \quad (\text{II-4})$$

$$\text{and } \bar{P} = (\bar{p}_1, \dots, \bar{p}_n) ; \bar{p}_i = \frac{x_i + 1}{m_i + 2} \quad (\text{II-5})$$

That is,

$$\Psi = \{A \mid f(\bar{A}) \leq f(\bar{P})\} . \quad (\text{II-6})$$

For example, in two dimensions the index set  $\Psi$  would contain all pairs of integers  $(a_1, a_2)$  so that the function values obtained by evaluating  $f$  at each of these pairs would fall under the curve  $f(\bar{p}_1, \bar{p}_2)$ . In this sense, we sometimes speak of the pairs as points lying under the curve  $f(\bar{p}_1, \bar{p}_2)$ . In three dimensions we are dealing with surface functions and for problems of dimension  $n > 3$  we write in terms of hypersurfaces.

### III. Hypervolumes and the Index Set

Theoretically, there is no reason not to evaluate  $H$  directly from (II-3). Practically, the use of (II-3) in the many times that  $H$  must be evaluated results in an unacceptably long computer run time for the maximization search routine. It has proved possible to develop a more efficient method of evaluating  $H$ .

The discussion to follow has three segments. We first describe, in an intuitive manner, the various elemental ideas used in the construction of the set  $\Psi$  utilized for indexing in (II-3) and the development of hypervolumes. For those readers interested in hypervolumes only from the standpoint of how they relate to the problem of probability function maximization and not an in-depth analysis, this intuitive approach should suffice and not particularly detract from the discussions in later sections. Following this description are a rigorous development of hypervolumes and their properties, as well as a detailed algorithm for the index set construction based on that development.

From the simplified example given at the end of the previous section, we note that in two dimensions the index set  $\Psi$  would be composed of pairs of integers satisfying the set criteria of (II-6). Given a specific system failure probability function  $f$ , Figure 1 displays the single failure probability curve  $f(\bar{p}_1, \bar{p}_2)$  that might be associated with the component failure probabilities of  $\bar{p}_1$  and  $\bar{p}_2$  described by (II-5). However, the values  $\bar{p}_1$  and  $\bar{p}_2$  are dependent

upon the integer values  $x_1$  and  $x_2$  in the numerator of (II-5). Except in the "trivial" case where  $x_1 = x_2 = 0$ , other integer values substituted for  $x_1$  and  $x_2$ , simultaneously, could produce a function value coinciding with this curve or located somewhere below the curve. For the trivial case, only one pair of integers will accomplish this fact; namely, the pair (0,0). To distinguish the specific test situation identified by  $\bar{p}_1$  and  $\bar{p}_2$ , we make use of a similar notation (II-4) where these additional integer values may be considered.

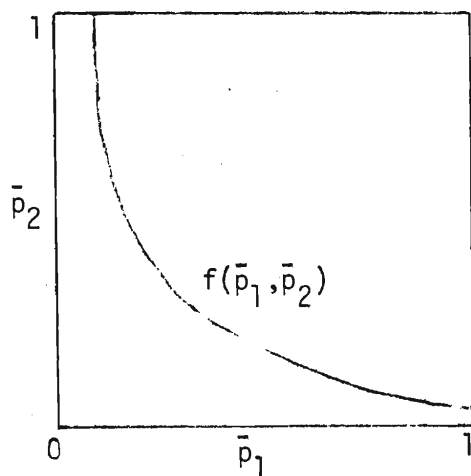
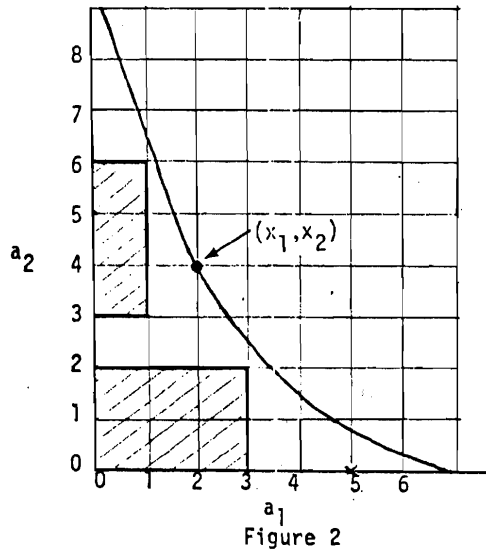


Figure 1.

In a sense, the  $p$  component values are scaled values of integers. From this standpoint we can envision the curve overlying a graph of integers or a lattice of integers. Figure 2 illustrates such a lattice possible for some particular two-dimensional problem.



For the illustration, the pairs of integers  $(a_1, a_2)$  yielding function values,  $f(\bar{a}_1, \bar{a}_2)$ , below the curve would consist of

- (0,0) (1,0) (2,0) (3,0) (4,0) (5,0) (6,0)
- (0,1) (1,1) (2,1) (3,1) (4,1)
- (0,2) (1,2) (2,2) (3,2) (4,2)
- ⋮     ⋮
- (0,6) (1,6)
- (0,7)
- (0,8)

In order to express these pairs in a more compact notation, save storage space within a computer program, reduce the necessary time to determine all points satisfying (II-6), and develop the constraint equation (II-3) into a more efficient and usable form, we utilize the terminology of hypervolumes. A hypervolume, designated as HV, can be described simply as a rectangle, parallelepiped, etc., respectively, as the number of dimensions increase. Thus, in our example, we can describe all points ranging from 0 to 3 in  $a_1$  and 0 to 2 in  $a_2$  as belonging to the first



hypervolume,  $HV_1 = \{[0,3], [0,2]\}$ . This rectangle is shown in Figure 2. A second hypervolume,  $HV_2 = \{[0,1], [3,6]\}$  is also shown in Figure 2. Notice that we did not touch rectangles, since they would have overlapped on the two points (0,2) and (1,2). If one keeps in mind the idea that we want to express lattice points in a new terminology and that dimension only places an upper bound on the geometric form a hypervolume can assume, it will not be difficult to see that a third hypervolume might consist of a line, e.g.,  $HV_3 = \{[4,4], [0,1]\} = (4,0), (4,1)$ , or a single point,  $HV_4 = \{[5,5], [0,0]\} = (5,0)$ .

In this manner, we can include all points of the underlying lattice in the hypervolume form of definition. Upon insuring that there are no overlapping points (i.e., maintaining unique hypervolumes), we then have the necessary index set  $\Psi$  of (II-3) whereby the total union of the hypervolumes compose  $\Psi$ . The discussion up to this point has been primarily concerned with two-dimensional situations, but the general idea of describing clusters of lattice points in a compact form can be carried through for higher dimensions.

To effectively define and describe a generalized approach of hypervolume construction and yet implement an algorithm in a practical and logical sequence, we must undertake a more rigorous analysis. We assume the notation of (II-1) throughout the remaining discussion.

Definition 1: Given a set of numbers  $\{m_1, m_2, \dots, m_n\}$  denoting the number of tests performed on each component, a choice space  $X$  of dimension  $n$  is defined to be the set of all points  $A = (a_1, a_2, \dots, a_n)$  so that  $0 \leq a_1 \leq m_1, 0 \leq a_2 \leq m_2, \dots, 0 \leq a_n \leq m_n$ . With the dimensionality of a point  $A \in X$  implied, the term point is taken to be synonymous with the term n-tuple.

From this definition and equation (II-4) we see that  $\Psi \subset X$ . As the dimension increases (i.e., larger systems) and each of the  $m_i$  also increases, the procedure to be used in determining the contents of the index set  $\Psi$  can become extremely time consuming. Furthermore,  $\Psi$  must be constructed so that repeated evaluations of equations similar to (II-3) can be made as efficiently as possible.

During these studies, several schemes were devised for the construction of  $\Psi$  to determine the elements  $A \in \Psi$ . Although one approach devised by Mueller was deemed more efficient than others, having several algorithms available proved beneficial in checking the contents of  $\Psi$ . We shall designate the method of construction utilized for  $\Psi$  as the "hypervolume algorithm." To lay the foundation for subsequent discussion and development, we begin the description of the method of construction in a formal manner.

Definition 2: If  $(a_1, \dots, a_k, \dots, a_n)$  is an n-tuple, then the closed set of integers along the kth component coordinate for which  $a_k$  may range is designated as  $R_k$ . Thus,  $R_k$  is the set of integers ranging from a minimum value or lower limit,  $L_k$ , to a maximum value or upper limit,  $U_k$ , and  $R_k = [L_k, U_k]$ .

Definition 3: A hypervolume HV in the choice space X of dimension n is defined to be the set of points

$$HV = \left\{ (a_1, \dots, a_k, \dots, a_n) \mid a_1 \in R_1, \dots, a_k \in R_k, \dots, a_n \in R_n \right\} .$$

A reduced form of notation to be used is

$$HV = \left\{ R_1, \dots, R_k, \dots, R_n \right\} .$$

From Definition 3, we see that each component  $a_k$  in an n-tuple has a definite range of values for a particular hypervolume. In a sense, this range represents an edge of the hypervolume being described. When taken together with the other components, the hypervolume then becomes filled with points. The next three definitions provide us with the means to distinguish between unique hypervolumes.

Definition 4: The hypervolume  $HV_i$  indicates the ith hypervolume in the space and is defined as

$$\begin{aligned} HV_i &= \left\{ R_1(i), \dots, R_n(i) \right\} \\ &= \left\{ [L_1(i), U_1(i)] , \dots, [L_n(i), U_n(i)] \right\} . \end{aligned}$$

Let us consider an example where there are two unique components to a system under study. In examining the components, suppose that 50 observations were made of the first component and for the second component 47 observations were made. Hence,  $n = 2$ ,  $m_1 = 50$ ,  $m_2 = 47$  and  $X = \{(a_1, a_2) \mid 0 \leq a_1 \leq 50, 0 \leq a_2 \leq 47\}$ .

With these conditions, we might have hypervolumes such as

$$HV_1 = \{[0, 2], [0, 3]\} \text{ or } HV_2 = \{[1, 3], [2, 6]\} .$$

There would be 12 points in  $HV_1$ :

$$\begin{array}{cccc} (0, 0) , & (0, 1) , & (0, 2) , & (0, 3) \\ (1, 0) , & (1, 1) , & (1, 2) , & (1, 3) \\ (2, 0) , & (2, 1) , & (2, 2) , & (2, 3) . \end{array}$$

Similarly, there would be 15 points in  $HV_2$ .

Definition 5: Two points  $A_1$  and  $A_2$  in the space  $X$  coincide,  $A_1 \equiv A_2$ , iff all components of the points are equal.

Definition 6: Hypervolumes  $HV_i$  and  $HV_j$  do not overlap in the  $k^{\text{th}}$  dimension when  $U_k(i) < L_k(j)$  or  $L_k(i) > U_k(j)$ . We define the symbol  $R_k(i) // R_k(j)$  to denote this relationship..

Theorem 1: If  $R_k(i) // R_k(j)$  for any  $k$ , then the two hypervolumes  $HV_i$  and  $HV_j$  have no common points,

$$HV_i \cap HV_j = \emptyset .$$

Proof: Consider some point  $A \in HV_i$ ,  $A = (a_1, \dots, a_n)$ . Then, by definition of hypervolumes,  $a_k \notin [L_k(i), U_k(i)]$  for each  $k$  and we have

$$(1) \quad R_k(i) // R_k(j) \Rightarrow U_k(i) < L_k(j) \Rightarrow a_k < L_k(j) \Rightarrow a_k \notin [L_k(j), U_k(j)] ,$$

or

$$(2) \quad R_k(i) // R_k(j) \Rightarrow L_k(i) > U_k(j) \Rightarrow a_k > U_k(j) \Rightarrow a_k \notin [L_k(j), U_k(j)] .$$

But  $a_k \notin [L_k(j), U_k(j)] \Rightarrow A \notin HV_j$  and therefore

$$HV_i \cap HV_j = \emptyset . \blacksquare$$

The theorem shows us that if one questions whether two hypervolumes have any points in common we need only find a single coordinate in which  $R_k(i) // R_k(j)$ , and there will be no common points.

Corollary: Two hypervolumes overlap if there exists at least one coincident point of the hypervolumes.

Proof: Consider two points in the space  $X$ ,

$$A_1 = (a_1, \dots, a_k, \dots, a_n) \text{ and } A_2 = (a'_1, \dots, a'_k, \dots, a'_n) .$$

Then

$$A_1 \in HV_i \cap HV_j$$

$$\Leftrightarrow A_1 \in HV_i \text{ and } A_1 \in HV_j$$

$$\Leftrightarrow a_k \in R_k(i) \text{ and } a_k \in R_k(j), \forall k$$

$$\Leftrightarrow a_k = \text{a component } a'_k \in R_k(j), \forall k$$

$$\Leftrightarrow (a_1, \dots, a_k, \dots, a_n) \equiv (a'_1, \dots, a'_k, \dots, a'_n)$$

$$\Leftrightarrow A_1 \equiv A_2. \blacksquare$$

Definition 7: A hypervolume  $HV_i$  is said to be a subset of another hypervolume  $HV_j$  iff

$$U_k(i) \leq U_k(j) \text{ and } L_k(i) \geq L_k(j), \forall k.$$

We denote this relation by  $HV_i \subset HV_j$ . We also refer to containment within a single coordinate  $k$  as  $R_k(i) \subset R_k(j)$  so that  $\forall k, R_k(i) \subset R_k(j) \Leftrightarrow HV_i \subset HV_j$ .

Note that when  $HV_i \subset HV_j$ , one hypervolume is completely contained within another. That is,  $HV_i \cap HV_j = HV_i$ . It may also be the case that the two hypervolumes are identical. By Theorem 1,  $R_k(i) // R_k(j)$  for any  $k \Rightarrow HV_i \not\subset HV_j$ . Let us examine situations whereby there may be overlap between two hypervolumes, but not complete containment.

Definition 8: A hypervolume  $HV_i$  is said to be free from overlap at the lower end in the  $k$ -dimension relative to some other hypervolume  $HV_j$  iff

$$L_k(j) \leq U_k(i) \leq U_k(j) \text{ and } L_k(i) < L_k(j).$$

We define the symbol  $R_k(i) \underline{0} R_k(j)$  to denote this relation.

Theorem 2: Let  $HV_i$  and  $HV_j$  be any two hypervolumes in  $X$ . If  $R_m(i) \underline{0} R_m(j)$  for one or more  $m$ , then redefining  $HV_i$  so that  $U_m(i) = L_m(j) - 1$  for any single  $m$  yields  $HV_i \cap HV_j = \emptyset$ .

$$\text{Proof: } U_m(i) = L_m(j) - 1 \Rightarrow U_m(i) < L_m(j) \Rightarrow R_m(i) // R_m(j)$$

and from Theorem 1,  $HV_i \cap HV_j = \emptyset. \blacksquare$

Definition 9: A hypervolume  $HV_i$  is said to be free from overlap at the upper end in the  $k$ -dimension relative to some other hypervolume  $HV_j$  iff

$$U_k(i) > U_k(j) \text{ and } L_k(i) \leq U_k(j).$$

We define the symbol  $R_k(i) \bar{\cap} R_k(j)$  to denote this relation.

Note that in the relation  $R_k(i) \bar{\cap} R_k(j)$  there is no restriction on the location of the lower bound  $L_k(j)$ , and thus  $R_k(i) \bar{\cap} R_k(j)$  cannot be considered the inverse of  $R_k(i) \underline{\cap} R_k(j)$ . That is,  $R_k(i) \bar{\cap} R_k(j)$  allows the possibility of overlap at both ends.

Theorem 3: Let  $HV_i$  and  $HV_j$  be any two hypervolumes in  $X$ . If  $R_m(i) \bar{\cap} R_m(j)$  for one or more  $m$ , then redefining  $HV_i$  so that  $L_m(i) = U_m(j) + 1$  for any single  $m$  yields  $HV_i \cap HV_j = \emptyset$ .

Proof:  $L_m(i) = U_m(j) + 1 \Rightarrow L_m(i) > U_m(j) \Rightarrow R_m(i) // R_m(j)$  and from

Theorem 1,  $HV_i \cap HV_j = \emptyset$ . ■

The construction of the index set  $\Psi$  is based upon the preceding definitions and theorems. Acceptance of a hypervolume for possible inclusion in  $\Psi$  is governed by the criterion that the hypervolume bounds satisfy Equation (II-6). By determining all unique hypervolumes under the function surface,  $HV_j$ ,  $j=1, \dots, M$  we have

$$\Psi = \bigcup_{j=1}^M HV_j \text{ and } \bigcap_{j=1}^M HV_j = \emptyset.$$

Aligning the hypervolumes along one coordinate axis enables a uniform search procedure. That is, the minimum value of the first coordinate in each hypervolume remains fixed at zero, since all hypervolumes must fall under the function surface and extend from each axis out toward the function surface.

We begin the construction by defining a set of numbers  $\{L_1^*, L_2^*, \dots, L_n^*\}$  which contains the minimum values each hypervolume coordinate can respectively assume at the most current step in the search procedure. Essentially, these starred values maintain a log of where a new volume can be located. This process will become more apparent as we move through the method description. Initially we define  $L_k^* = 0, k=1, \dots, n$ . The value  $L_1^*$  remains locked at zero as mentioned above, while all others vary as the construction proceeds.

For clarity in the following explanation, each step in the construction process is numbered. Branching is indicated at appropriate places for comparisons or tests, to take alternative action, or to begin new cycles. The bounds of a hypervolume are determined by starting at a single point in the space and then stepping out in each of the coordinate directions to encompass as much volume as possible and still satisfy the function surface criterion.

Let  $i$  indicate the index of the current hypervolume being constructed; initially  $i=1$ .

1. Set  $U_1(i)$  to the largest  $a_1$  for which

$$(a_1, L_2^*, L_3^*, \dots, L_n^*) \in \Psi, U_1(i) \geq L_1^* \equiv 0.$$



2. Set  $U_2(i)$  to the largest  $a_2$  for which

$$(U_1(i), a_2, L_3^*, L_4^*, \dots, L_n^*) \in \Psi, U_2(i) \geq L_2^* .$$

3. Set  $U_k(i)$  to the largest  $a_k$  for which

$$(U_1(i), \dots, U_{k-1}(i), a_k, L_{k+1}^*, L_{k+2}^*, \dots, L_n^*) \in \Psi,$$

$$U_k \geq L_k^* \text{ with repeated looping on } k \text{ where } k=3, \dots, n.$$

4. Set  $L_k(i) = L_k^*, k=1, \dots, n$ . Note that  $L_1(i) \equiv L_1^* \equiv 0$ .

At this point in the algorithm a hypervolume has been defined, but may not be uniquely different from previously defined hypervolumes. That is, this new hypervolume must be pairwise disjoint with all previously defined hypervolumes before accepted into the index set  $\Psi$ . For this reason, the hypervolume must be checked against all other hypervolumes constructed. Holding  $HV_i$  fixed ( $i > 1$ ), each  $HV_j, j=1, \dots, i-1$  is compared coordinate by coordinate. For any given coordinate  $k$ , one and only one of the following relations will hold:

$$(a). R_k(i) // R_k(j) \quad (\text{Definition 6})$$

$$(b). R_k(i) \subset R_k(j) \quad (\text{Definition 7})$$

$$(c). R_k(i) \underline{\cap} R_k(j) \quad (\text{Definition 8})$$

$$(d). R_k(i) \bar{\cap} R_k(j) \quad (\text{Definition 9})$$

5. Looping on the coordinate index  $k$ ,  $k=1, \dots, n$  compare hypervolume  $HV_i$  with hypervolume  $HV_j$  for one of the possible conditions described above.
- (a). If  $R_k(i) // R_k(j)$  for any  $k$ , then by Theorem 1  $HV_i \cap HV_j = \emptyset$ .  
Go to step 6.
- (b). If  $R_k(i) \subset R_k(j)$  for all  $k$ , then by Definition 7,  $HV_i \subset HV_j$  and  $HV_i$  cannot be included in  $\Psi$ . Go to step 8.
- (c). If  $R_k(i) \underline{0} R_k(j)$  for one or more  $k$ , then by Theorem 2 we can redefine  $HV_i$  so that  $HV_i \cap HV_j = \emptyset$ . Before redefining  $HV_i$  we must insure that condition (a) does not already exist. Thus, all coordinates in  $HV_i$  must be compared with those of  $HV_j$ . From Theorem 2, only one coordinate in  $HV_i$  should be redefined. Let  $m$  be the last coordinate for which  $R_m(i) \underline{0} R_m(j)$ . Set  $U_m(i) = L_m(j) - 1$  and go to step 6.
- (d). If  $R_k(i) \overline{0} R_k(j)$  for one or more  $k$ , then by Theorem 3 we can redefine  $HV_i$  so that  $HV_i \cap HV_j = \emptyset$ . All coordinates in  $HV_i$  must be compared with those of  $HV_j$  to insure that condition (a) does not already exist. We may also have the situation where  $\overline{0}$  exists for one coordinate and  $\underline{0}$  for another coordinate. If so, go to 5c. If not, then let  $m$  be the last coordinate for which  $R_m(i) \overline{0} R_m(j)$  and set  $L_m(i) = U_m(j) + 1$ . Go on to step 6.
6. Hypervolume  $HV_i$  is disjoint with  $HV_j$ . Increment  $j$  to  $j+1$ . If  $j+1 < i$  go to step 5 for comparison of  $HV_i$  with the next hypervolume. If  $j+1 = i$ ,

all comparisons have been made and we have  $HV_i \cap HV_j = \emptyset$ ,  $j=1, \dots, i-1$ . Store the bounds of  $HV_i$ ,  $L_1(i), \dots, L_n(i)$  and  $U_1(i), \dots, U_n(i)$  to represent a new and acceptable hypervolume. Proceed to step 7.

7. With a new hypervolume accepted, the starred variables must reflect the new minimums acceptable in locating the next hypervolume.

$$\text{Set } L_2^* = \text{Max. } \{L_2^*, U_2(i)\} + 1 = U_2(i) + 1.$$

Hold  $L_3^*, \dots, L_n^*$  fixed.  $L_1^* \equiv 0$ . Increment  $i$  to  $i+1$  and go to step 9.

8. The hypervolume being tested for possible inclusion was already covered.

Set  $L_2^* = \text{Max. } \{L_2^*, U_2(i)\} + 1 = U_2(i) + 1$ . Do not increment  $i$ . Go to step 9.

9. If  $(0, L_2^*, L_3^*, \dots, L_n^*) \in \Psi$ , go to step 1 and begin construction of the next hypervolume.

If  $(0, L_2^*, L_3^*, \dots, L_n^*) \notin \Psi$ , set  $L_2^* = 0$  and  $L_3^* = \text{Min. } \{U_3(j) \mid U_3(j) \geq L_3^*, j=1, \dots, i\} + 1$ .

Go to Step 10.

10. If  $(0, L_2^* = 0, L_3^*, L_4^*, \dots, L_n^*) \in \Psi$ , go to 1. Otherwise, set  $L_3^* = 0$  and  $L_4^* = \text{Min. } \{U_4(j) \mid U_4(j) \geq L_4^*, j=1, \dots, i\} + 1$ . Go on to step 11.

11. The procedure continues as described in steps 9 and 10. Looping on  $k$ ,  $k=3, \dots, n-1$ , if  $(0, L_2^*, \dots, L_n^*) \in \Psi$ , go to 1. Otherwise, set  $L_k^* = 0$  and  $L_{k+1}^* = \text{Min. } \{U_{k+1}(j) \mid U_{k+1}(j) \geq L_{k+1}^*, j=1, \dots, i\} + 1$ .

Note that if there exists a value  $U_{k+1}(j) = L_{k+1}^*$  we can immediately define the new  $L_{k+1}^*$  without further testing in this coordinate. Check the new starred point for containment in  $\Psi$ .

12. A point will be reached when, through all the searching,  $L_k^* = 0$ ,  $k=1, \dots, n-1$  and  $(0, 0, \dots, 0, L_k^*) \notin \Psi$ . The next logical step would be to define  $L_n^* = 0$ , but this returns us to the very first starting point. Hence, the construction has been completed with  $i-1$  hypervolumes in  $\Psi$ .

In the construction algorithm, we note in steps 9, 10, and 11 that there exists at least one value  $U_k(j)$  so that  $U_k(j) \geq L_k^*$ ; namely, the most recent upper bound determined in this dimension as so defined in steps 1, 2, or 3. Furthermore, since it may well be that this most recent upper bound is equal to  $L_k^*$  and the new  $L_k^*$  could be immediately defined without further checking, a descending search with  $j=i, i-1, \dots, 1$  is most expedient.

As remarked earlier, several different approaches were planned and written for the construction of  $\Psi$ . The advantages in doing so were twofold. First, insight and understanding of the problems of construction were gained which ultimately led to the method of hypervolumes. Questions such as how to present the index set most uniformly and concisely for explanation, how equations could most effectively be redesigned for efficient evaluation, and how systems of differing dimensions and sizes could be compared were more easily answered.

The other advantage in having different approaches was the ability to check the components of index sets for various systems. The method of construction

used in comparison testing was one in which all the n-tuple components were found one at a time. This method can be described somewhat analogously by the operation of an odometer. That is, each coordinate assumed a "register" position. All registers started at zero and operated from right to left (nth coordinate to 1st coordinate). A coordinate register value would increment until reaching the criterion function acceptance value, at which time a pointer moved to the next register in sequence and the previously used registers would restart at zero. This search method continued until all registers had moved to their maximum acceptable limit. During each step the current register readings were recorded and thus the total n-tuple readings made up the index set.

Tests were performed on various systems ranging from two to six dimensions, and one system of nine dimensions. In all instances, the index sets constructed by the hypervolume method were exactly the same as those constructed by the register method.

Apart from the comparison checks, other tests were performed. Defining the number of failures found in each system as zero (i.e.,  $x_i = 0, i=1, \dots, n$ ), several different systems were analyzed and each index set was determined. As desired, each set did consist of the single n-tuple  $(0, 0, \dots, 0)$ .

Another type of checking done was to consider subsets of index sets. Given a particular system with some number of failures input,  $x_i, i=1, \dots, n$ , a corresponding index set was found. Then by reducing the number of failure values input, other index sets were determined. In each case tested, the

smaller index set was completely contained by the larger set. This test was repeated several times for the systems ranging from two to six dimensions, as well as for the nine-dimensional system.

A slightly different approach was to select some n-tuple within a given index set as input to the system under consideration. As expected, the new resulting index set in each case was a subset of the original set and included all of the proper n-tuples.

The use of hypervolumes presents a concise and uniform method of describing the index set  $\Psi$ . As will be seen in the following section of this report, the most important feature of the method of hypervolumes is the very efficient manner in which complex equations such as (II-3) can be evaluated.

#### IV. Nonlinear Function Maximization

The problem of finding the maximum of a nonlinear function of several variables with nonlinear constraints is well known in numerical analysis. Considerable attention has been given to the minimization of nonlinear functions and several different approaches have been proposed [2]. Although normally posed in terms of minimization, by making a few minor changes the methods apply to maximization as well. In nearly all of the techniques proposed, the partial derivatives of the given function to be maximized, with respect to each independent variable, are necessary to provide input as to the direction of greatest change [3] and as a measure of the convergence process [4].

Considering the fact that we are concerned with probability functions involving several-to-many variables,  $f(p_1, \dots, p_n)$ , the requirement for partial derivatives becomes rather undesirable. This undesirability is further magnified, since the user of the general CONLIM computer program is responsible for supplying the function to be maximized. To circumvent these difficulties, we propose a modified univariate method; i.e., changing one variable at a time.

Since both  $f$  and the  $p$  values are probabilities, they must satisfy the conditions

$$0 \leq f(p_1, \dots, p_n) \leq 1 \quad (\text{IV-1})$$

and

$$0 \leq p_i \leq 1, \quad i = 1, \dots, n.$$

For ease of illustration, diagrams supplied will be in terms of only two dimensions, but the theory and application hold for higher dimensions and have been used in this context. Hence, in two dimensions we can view the function  $f$  as a family of curves dependent upon the two variables  $p_1$  and  $p_2$ . Figure 3 illustrates a possible configuration of the function curves and the constraint curve  $H(p_1, p_2) = 1 - \alpha$ . We search for the point

at which the curve  $H = 1 - \alpha$  is tangent to the curve  $f_k$ . The value of  $f_k$  is then the confidence limit we are seeking.

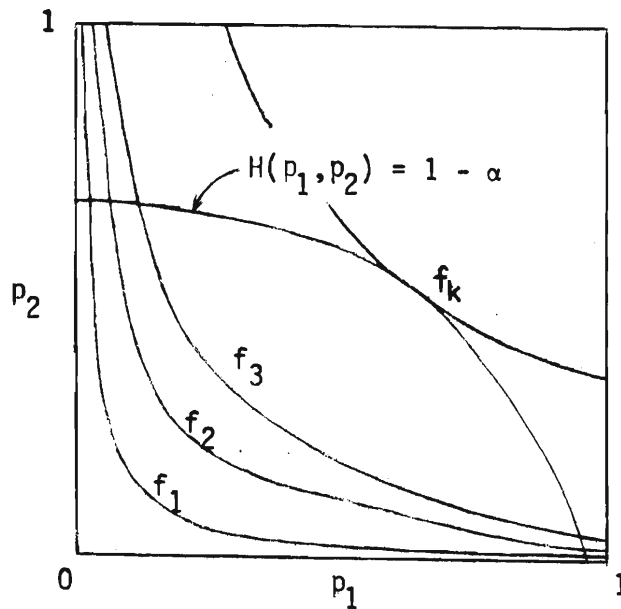


Figure 3

The search is initiated from the point

$$\bar{P} = (\bar{p}_1, \dots, \bar{p}_n) \quad , \quad \bar{p}_i = \frac{x_i + 1}{m_i + 2} \quad , \quad x_i \leq m_i \quad ;$$

(IV-2)

$i = 1, \dots, n$  .

By using Steck's iterative procedure [ 1 ] for an index set, one obtains the global maximum function value. But we wish to avoid an impractically long iteration process to determine this set. Differing from Steck's approach, we admit tie points in the set ordering. The starting point  $\bar{P}$  was chosen by Müller to direct the search toward a maximum judged to correspond most closely with the global. However, the search routine could conceivably find a local maximum rather than the global maximum. When this occurs, it is as though we are saying that the index set generated is not producing the ordering we want and we effectively reject (or ignore) those points in the



ordering which would create a global maximum elsewhere. The contribution of those "global" points at the local maximum is very small, so the value of the local maximum is affected very little by whether they are, or are not, a part of the ordering. This has the unsettling aspect that we cannot precisely define in mathematical terms the ordering we are using, but the ordering is uniquely and precisely defined by the computer algorithm. The point is that any definite, repeatable ordering will produce a valid system of confidence limits, and we have such an ordering judged to be, if anything, somewhat better than the implied ordering identified by the index set.

With reference to Fig. 4, the procedure of maximization to be used will first be briefly described for an overview and then discussed in detail. Note that initially the  $\bar{p}_i$  values are held away from the end (boundary) conditions so that  $0 < \bar{p}_i < 1$ .

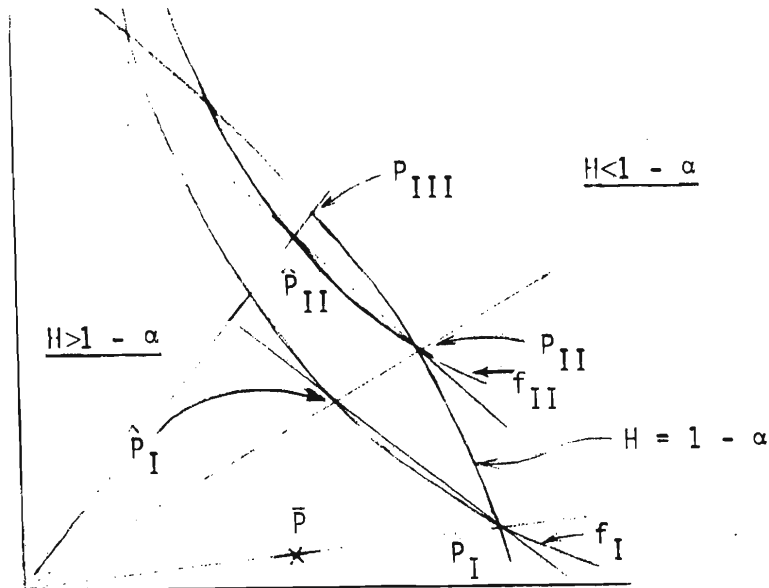


Figure 4

The computational complexity of the H function and the extreme amount of time that would be required for many evaluations of H preclude moving along the curve  $H = 1 - \alpha$  to find the maximum of f. Consequently, we have

followed the suggestion of Müller and "inverted" the maximization procedure. From the initial point  $\bar{P}$  we move to the  $1 - \alpha$  constraint curve along a line intersecting  $\bar{P}$  and the origin. In so doing, the point  $P_I = (p_1, \dots, p_n)_I$  on the  $1 - \alpha$  curve is obtained and we then calculate the corresponding function value  $f(P_I)$ . A step of appropriate length,  $\delta_1$ , is taken to the point  $\hat{P}_I$  along a constant  $f$  curve (i.e.,  $f_I = f(P_I) = C$ ), in the direction of increasing  $H$  values. From  $\hat{P}_I$  we return to the  $1 - \alpha$  curve at the point  $P_{II}$  directly away from the origin. Since  $H$  is monotonically decreasing away from the origin while  $F$  is monotonically increasing away from the origin, the new point  $P_{II}$  will have a larger  $f$  value than that for  $P_I$ ; i.e.,  $f(P_{II}) > f(P_I)$ . Thus the general direction of new point placement is toward the interior of the envelope formed between  $H = 1 - \alpha$  and  $f_I$ . After determining  $f_{II}$ , the next function curve to be held constant, the same procedure is repeated. This iterative process is continued until a step with fixed  $\delta$  is found to produce a corresponding  $H$  value less than the  $H$  value before the step was taken; i.e., until the step places the next point outside the current envelope and beyond the intersection of the constant  $1 - \alpha$  and  $f$  curves. The step size is then reduced to  $\delta_2 = \delta_1/2$  and the iteration continued. When the step size has been reduced to some value  $\delta_k = \delta_{k-1}/2 < 10^{-d}$ , where  $d$  is the number of digits at which the variables  $p_i$  are to be affected by the steps, the entire procedure is halted. Through this inverted method the function  $f$  evaluated at the last point,  $P^*$ , on the  $H = 1 - \alpha$  curve produces the desired maximum of the function. The number of evaluations of  $H$  required by this approach is significantly reduced since  $H$  is only computed in each cycle to establish direction and to return to  $1 - \alpha$  from the constant  $f$  curves.

Keeping in mind the procedure just described, we now detail the equations and formulation necessary to carry out these operations. During each part of the iteration, we select some point  $\hat{P}_j = (\hat{p}_1, \dots, \hat{p}_n)_j$  away from the  $1 - \alpha$  constraint curve that increases the value of  $H$  and places us toward the center of the envelope. Each point  $\hat{P}_j$  is forced to maintain a constant function value  $f_j$ ; i.e., movement to the point  $\hat{P}_j$  is along the  $f_j$  curve. To enable such a movement, we place a restriction on the system, and thus on the function  $f$ . Each component of the system can be described

as connected in series or parallel with the other components. The system is restricted in that it must contain at least one series connected component. In Fig. 5, let  $Q$  represent the failure probability accumulated over  $n - 1$  components, and  $p_n$  represent the failure probability of a single series component. We simply remark at this point in the discussion that when there exists more than one series component in the system, that  $p_n$  represents the series component probability of greatest value within the immediate step cycle. The subscript  $n$  is used to distinguish that component and the corresponding value from the remainder of the system, and does not necessarily indicate the final system component. For clarification and future reference, we shall henceforth refer to the series component considered separately in each cycle as the "slack" component since it is essentially used to take up the slack in holding to a constant  $f$  curve.



Figure 5

Then the failure probability of the system becomes

$$\begin{aligned}
 f &= 1 - [(1 - Q)(1 - p_n)] \\
 &= Q + p_n (1 - Q)
 \end{aligned}
 \tag{IV-3}$$

Incrementing a parallel component by a relatively large step value produces approximately the same function incrementation as when a series component is only slightly modified. Hence, two separate step values,  $\delta_s$  for series components and  $\delta_p$  for parallel, are maintained. A too-small initial step would result in many cycles of maximization and increased computer time, and a very large start might overstep the envelope and possibly influence the direction of movement, initially, away from the maximum. In

terms of an optimum first step size, experience has shown the initial step values to be best defined as

$$\delta_s = \left( \sum_{i=1}^n \bar{p}_i \right) / 10 n, \quad \delta_p = \sqrt{\delta_s} .$$

The series components are affected, at most, in the second decimal place and parallel components in the first or second place, depending on the average  $\bar{p}$  values. In the following discussion, the step size will always be referred to in the generic sense,  $\delta$ , with the actual value used assumed dependent upon the component designation.

Starting on the constraint curve in the  $j$ th iteration ( $j = 1, \dots, M$ ) with a given point  $P_j = (p_1, \dots, p_n)_j$ , we calculate the intersecting function value  $f(P_j)$  providing the "constant" curve along which a new point  $\hat{P}_j = (\hat{p}_1, \dots, \hat{p}_n)_j$  is to be found. The variable  $p_{n-1}$  is modified by some step value  $\delta$  so that  $\hat{p}_{n-1} = p_{n-1} + \delta$  and all other variables,  $p_i, i \neq n-1$ , are left unchanged. From the series restriction on the slack component we can insure this step to fall on the "f-constant" curve by using (IV-3) to give

$$\hat{p}_n = \frac{f(P_j) - Q(p_1, p_2, \dots, \hat{p}_{n-1})}{1 - Q(p_1, p_2, \dots, \hat{p}_{n-1})} . \quad (\text{IV-4})$$

Hence, the slack component takes up the difference necessary to maintain  $f(P_j)$  and assumes the value  $\hat{p}_n$ .

The function  $H$  is evaluated for  $(p_1, p_2, \dots, \hat{p}_{n-1}, \hat{p}_n)$ . Should it be the case that we have violated the boundary condition (IV-1) or that  $H$  has decreased, the value of the slack component is set back to  $p_n$  and we try to step in the opposite direction,  $\hat{p}_{n-1} = p_{n-1} - \delta$ . A new value for  $\hat{p}_n$  is obtained from (IV-4) to hold to the curve and we again check this

value. Provided that (IV-1) is satisfied and H has increased,  $p_{n-1}$  becomes fixed at the new value  $\hat{p}_{n-1} = p_{n-1} \pm \delta$ . If (IV-1) is not satisfied,  $\hat{p}_{n-1} = p_{n-1}$ .

The univariate process continues by adjusting the next component  $p_{n-2}$ , with  $\delta$ . Modification of the slack component is again made to place the search point on the constant curve and (IV-1) is checked. However, we are also seeking to position the completely stepped point  $\hat{P}_j$  at the greatest value of  $H(\hat{P}_j)$  that can be obtained within the  $\delta$  step limit. Before accepting the value  $\hat{p}_{n-2} = p_{n-2} \pm \delta$  for this component, a comparison is made with the previously held position and we find that

$$\Delta H_{n-2} = H(p_1, p_2, \dots, \hat{p}_{n-2}, \hat{p}_{n-1}, \hat{p}_n) - H(p_1, p_2, \dots, p_{n-2}, \hat{p}_{n-1}, \hat{p}_n)$$

Based on this calculation the following selection is made:

$$\hat{p}_{n-2} = \begin{cases} p_{n-2} \pm \delta & \text{if } \Delta H_{n-2} \geq 0 \\ p_{n-2} & \text{if } \Delta H_{n-2} < 0 \end{cases}$$

Taking one coordinate at a time, the iteration proceeds until all  $n - 1$  components have been incremented, decremented, or left unchanged. At each step along the way the slack component is modified to hold the moving point on the constant curve, and also at each step the boundary condition (IV-1) is checked and a comparison made on the H function increase. In general, we can summarize the component values by

$$\hat{p}_i = \begin{cases} p_i \pm \delta & \text{if } H_i > 1 - \alpha ; \Delta H_i \geq 0 ; 0 \leq p_i \leq 1 ; 0 \leq \hat{p}_n \leq 1 \\ p_i & \text{otherwise} \end{cases} \quad (\text{IV-5})$$

$$i = 1, \dots, n - 1$$

and

$$\hat{p}_n = \hat{p}_{n-1}$$

where the designation  $\wedge_i$  above the slack component denotes that  $p_n$  has been modified  $i$  times, as described in the text and as seen in (IV-4).

Although not obvious at first, one can see that if the same series component is held fixed as the slack component throughout the entire maximization procedure there exists the possibility of exhausting whatever magnitude and contribution that component may yield. In the situation where one component must continually be forced to maintain the difference to follow a constant curve, a resultant zero probability would halt the procedure since there would no longer be values to use as slack. Stopping at this point would quite possibly result in an erroneous solution. Also, concern that an undesirable bias in movement could result from a single slack component leads us to the position that all series components be considered for the slack role. The condition that a **sizable adjustment** might be necessary to remain on a constant  $f$  curve dictates the slack component to be the largest series component going into a step cycle. This component is held as slack through the complete step cycle, but then allowed to be reconsidered after a return is made to the  $1 - \alpha$  curve.

Upon the completion of the univariate step procedure, a new point  $\hat{P}_j = (\hat{p}_1, \dots, \hat{p}_n)_j$  has been found so that

$$f(\hat{P}_j) = f(P_j) \text{ and } H(\hat{P}_j) > H(P_j) \quad . \quad (\text{IV-6})$$

With the point  $\hat{P}_j$  fixed, we can determine another point,  $P_{j+1}$ , on the curve  $1 - \alpha$  whose  $f$  value is greater (and therefore closer to the maximum) than  $f(P_j)$ . To do so,  $\hat{P}_j$  and the origin are aligned as shown in Fig. 6. The next point,  $P_{j+1}$ , is calculated via a first-order approximation of the  $H$  function.

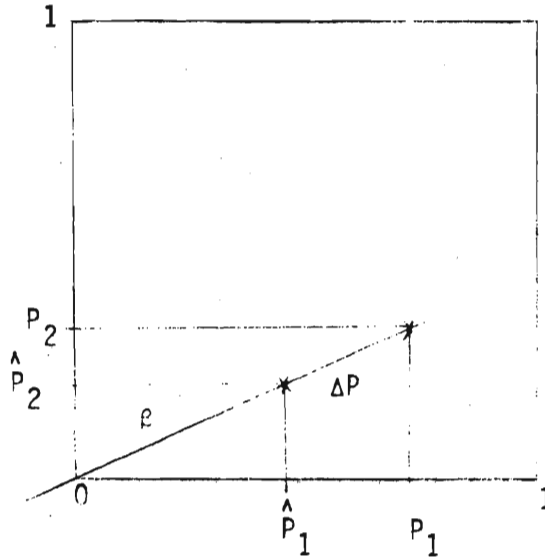


Figure 6.

Hence, for  $H(\hat{P}) > 1 - \alpha$ ,

$$\begin{aligned} p_i &= \hat{p}_i + (p_i - \hat{p}_i) \\ &= \hat{p}_i + \frac{\hat{p}_i}{\mathfrak{s}} \Delta p, \end{aligned} \quad (\text{IV-7})$$

where

$$\mathfrak{s} = \left\{ \sum_{k=1}^n \hat{p}_k^2 \right\}^{1/2}. \quad (\text{IV-8})$$

From equation (II-3) and the form of H, we have

$$H(P) = \sum_{\Psi} \prod_{i=1}^n \binom{m_i}{a_i} \left( \hat{p}_i + \hat{p}_i \frac{\Delta p}{\mathfrak{s}} \right)^{a_i} \left( 1 - \hat{p}_i + \hat{p}_i \frac{\Delta p}{\mathfrak{s}} \right)^{m_i - a_i}. \quad (\text{IV-9})$$

Expanding the first factor,

$$\left( \hat{p}_i + \hat{p}_i \frac{\Delta p}{\beta} \right)^{a_i} = \hat{p}_i^{a_i} + \binom{a_i}{1} \hat{p}_i^{a_i-1} \hat{p}_i \frac{\Delta p}{\beta} + \dots + \left( \hat{p}_i \frac{\Delta p}{\beta} \right)^{a_i}. \quad (\text{IV-10})$$

Similarly, expanding the second factor of (IV-9), we have

$$\begin{aligned} \left( 1 - \hat{p}_i + \hat{p}_i \frac{\Delta p}{-\beta} \right)^{m_i - a_i} &= \left( 1 - \hat{p}_i \right)^{m_i - a_i} + \binom{m_i - a_i}{1} \left( 1 - \hat{p}_i \right)^{m_i - a_i - 1} \hat{p}_i \frac{\Delta p}{-\beta} \\ &+ \dots + \left( \hat{p}_i \frac{\Delta p}{-\beta} \right)^{m_i - a_i}. \end{aligned} \quad (\text{IV-11})$$

By discarding all terms involving  $\Delta p^2$  and higher orders in (IV-10) and (IV-11), the two factors become

$$\begin{aligned} &\left[ \hat{p}_i^{a_i} + a_i \hat{p}_i^{a_i-1} \hat{p}_i \frac{\Delta p}{\beta} \right] \left[ \left( 1 - \hat{p}_i \right)^{m_i - a_i} + (m_i - a_i) \left( 1 - \hat{p}_i \right)^{m_i - a_i - 1} \hat{p}_i \frac{\Delta p}{-\beta} \right] \\ &= \hat{p}_i^{a_i} \left( 1 - \hat{p}_i \right)^{m_i - a_i} \left\{ 1 + \frac{\Delta p}{\beta} \left( \frac{a_i - m_i \hat{p}_i}{1 - \hat{p}_i} \right) \right\}. \end{aligned} \quad (\text{IV-12})$$

Substituting (IV-12) into (IV-9), we approximate H(P) by

$$H(P) \approx \sum_{\Psi} \prod_{i=1}^n \binom{m_i}{a_i} \hat{p}_i^{a_i} \left( 1 - \hat{p}_i \right)^{m_i - a_i} \left[ 1 + \frac{\Delta p}{\beta} \left( \frac{a_i - m_i \hat{p}_i}{1 - \hat{p}_i} \right) \right] \quad (\text{IV-13})$$

$$= \sum_{\Psi} \left\{ \prod_{i=1}^n \binom{m_i}{a_i} \hat{p}_i^{a_i} \left( 1 - \hat{p}_i \right)^{m_i - a_i} \right\} \left\{ \prod_{i=1}^n \left[ 1 + \frac{\Delta p}{\beta} \left( \frac{a_i - m_i \hat{p}_i}{1 - \hat{p}_i} \right) \right] \right\}.$$



Expanding the second product of (IV-13),

$$\prod_{i=1}^n \left[ 1 + \frac{\Delta p}{\beta} \left( \frac{a_i - m_i \hat{p}_i}{1 - \hat{p}_i} \right) \right] = 1 + \frac{\Delta p}{\beta} \sum_{i=1}^n \frac{a_i - m_i \hat{p}_i}{1 - \hat{p}_i} + \sum \text{Cross Product Terms} \quad (\text{IV-14})$$

Ignoring the cross product terms and substituting (IV-14) into (IV-13) gives

$$\begin{aligned} H(P) &\approx \sum_{\Psi} \left\{ \prod_{i=1}^n \binom{m_i}{a_i} \hat{p}_i^{a_i} (1 - \hat{p}_i)^{m_i - a_i} \right\} \left\{ 1 + \frac{\Delta p}{\beta} \sum_{i=1}^n \frac{a_i - m_i \hat{p}_i}{1 - \hat{p}_i} \right\} \\ &= \sum_{\Psi} \prod_{i=1}^n b_i + \frac{\Delta p}{\beta} \sum_{\Psi} \left( \prod_{i=1}^n b_i \right) \left( \sum_{i=1}^n c_i \right) \\ &= H(\hat{P}) + \frac{\Delta p}{\beta} B, \end{aligned} \quad (\text{IV-15})$$

where

$$B = \sum_{\Psi} \left( \prod_{i=1}^n b_i \right) \left( \sum_{i=1}^n c_i \right); \quad (\text{IV-16})$$

$$b_i = \binom{m_i}{a_i} \hat{p}_i^{a_i} (1 - \hat{p}_i)^{m_i - a_i}; \quad (\text{IV-17})$$

$$c_i = \frac{a_i - m_i \hat{p}_i}{1 - \hat{p}_i}. \quad (\text{IV-18})$$

The goal of this approximation is to obtain  $H(P) = 1 - \alpha$ , so that

$$1 - \alpha = H(\hat{P}) + \frac{\Delta p}{\beta} B$$

yielding

$$\Delta p = \frac{(1-\alpha) - H(\hat{P})}{B} \beta . \quad (\text{IV-19})$$

Substituting (IV-19) into (IV-7) gives

$$p_i = \hat{p}_i + \hat{p}_i \left[ \frac{(1-\alpha) - H(\hat{P})}{B} \right] . \quad (\text{IV-20})$$

Equation (IV-20) is also used to make the first step adjustment from the initial point estimate,  $\bar{P} = (\bar{p}_1, \dots, \bar{p}_n)$ , to the constraint curve provided that  $H(\bar{P}) > 1 - \alpha$ . However, it may well be the case that this point lies above the constraint curve; i.e.,  $H(\bar{P}) < 1 - \alpha$ . In this situation, equation (IV-7) should be modified to reflect the opposite direction:

$$p_i = \hat{p}_i - \frac{\hat{p}_i}{\beta} \Delta p = \hat{p}_i + \frac{\hat{p}_i}{-\beta} \Delta p .$$

But by substituting  $-\beta$  throughout the equations derived, we again obtain equation (IV-20). Equation (IV-20) is valid for both situations, since the denominator term  $B$  is negative in each case.

As in many other methods of maximization (minimization) there may arise the problem of oscillation with no progress made toward the maximum sought. Simply stated, this situation would occur when the step process becomes trapped on a curve,  $f$ , and an oscillation is encountered with slack components alternating or "vying" for direction control. In this situation, there are more than one local maximum, but only one such maximum appropriate for the system under study.

For example, a family of  $f$  curves containing a ripple or wave effect could lead the maximization procedure to "stall out" in that each new try to step to a greater  $f$  function value via (IV-20) only results in

positioning the new point on the opposite side of an f curve wave wall. As different slack components are utilized repeatedly to hold to this f curve it is evident that several paths to maximum values may exist. The immediate problem then becomes one of selecting the proper path to follow for the given system.

To recognize an oscillation, we maintain a survey of the pattern of slack components being used and, when a specific pattern is found to be repeating r times, a check on progress is made. If sufficient progress toward a maximum is taking place, then we do not want to interrupt the process but allow it to continue making progress. On the other hand, if very little or no progress is being made, then a junction exists and the different branches must be explored; i.e., we must force the maximization process to follow each branch path.

Let  $p_k$ ,  $k = 1, \dots, K$  represent the components being used in the slack role at the time of oscillation detection. The criteria for sufficient progress is established by examining the probability values of the slack component  $p_1$  held over this oscillation period,  $p_1^{(i)}$ ,  $i = 1, \dots, r$ . Remember that after any component values are modified by  $\delta$ , an adjustment is made through (IV-20) back to the constraint curve. If each value held by  $p_1$  during the period did not change more than one-half the current step size,  $\delta$ , then we indicate that a nonprogressing oscillation has occurred. That is, when

$$\left| p_1^{(i+1)} - p_1^{(i)} \right| < \delta/2, \quad i = 1, \dots, r - 1. \quad (\text{IV-21})$$

This situation dictates a slightly different approach to reach a global maximum. All p values, the current function value f, and the current H value are saved at the junction point and each path is then separately

followed through the maximization procedure but with a fixed slack component for each path. The process is illustrated in Fig. 7.

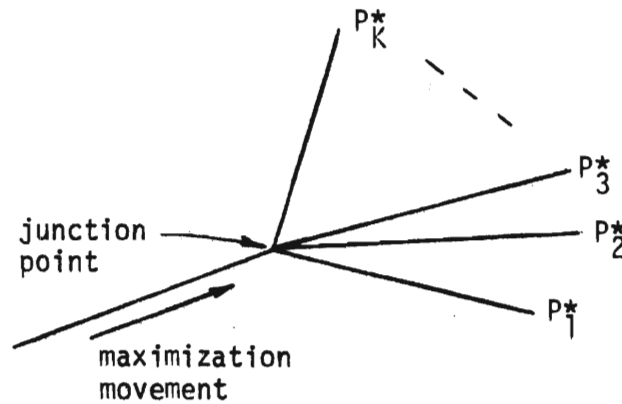


Figure 7.

Each point  $P_k^*$ ,  $k = 1, \dots, K$  reached is the maximum point satisfying (II-2) along the respective  $K$  paths taken. For the first path, slack component  $p_1$  is held as the only slack choice and no other components are considered for the slack role. The same procedure is followed for each  $k$ th path with the  $k$ th slack component fixed for that path. Each time a  $P_k^*$  maximum is obtained, the maximization procedure restarts at the junction point by picking up the saved junction values.

In the computer code, CONLIM, all  $P_k^*$  values are provided on output and the final selection of the "true" global maximum is left to the discretion of the code user. This method permits the user to consider the system structure, as well as any other exterior conditions, in making the selection. We note that in using CONLIM, the user has the option to not pursue any paths but rather to stop the problem at the junction point. Primary motivation for such a choice is the additional computer time necessary to complete the problem which would need to be weighed against the desirability of solution.

## V. Hypervolumes and the H-Function for Maximization

In a previous section, hypervolumes were defined and developed to form the index set  $\Psi$ . As the size of  $\Psi$  increases, the time to evaluate equations (II-3) and (IV-16) also increases. This time increase becomes magnified by the fact that larger systems require more evaluations of these two equations. Aside from the desire to be able to express  $\Psi$  compactly by means of hypervolumes, the other primary motivation for using hypervolumes is to facilitate the most efficient and rapid evaluation of these two major equations.

Expressing equation (II-3) in terms of summation over hypervolumes gives

$$H(P) = \sum_{j=1}^M \left\{ \sum_{A \in HV_j} \prod_{i=1}^n \binom{m_i}{a_i} p_i^{a_i} (1-p_i)^{m_i - a_i} \right\}. \quad (V-1)$$

Over each hypervolume  $HV_j$  we can factor the summation and product to obtain a reduced form so that

$$\begin{aligned} & \sum_{A \in HV_j} \prod_{i=1}^n \binom{m_i}{a_i} p_i^{a_i} (1-p_i)^{m_i - a_i} \\ &= \prod_{i=1}^n \sum_{k=\min_{ij}}^{\max_{ij}} \binom{m_i}{k} p_i^k (1-p_i)^{m_i - k}, \quad j=1, \dots, M, \quad (V-2) \end{aligned}$$

where  $\min_{ij}$  = minimum value of  $i$ th coordinate,  $j$ th hypervolume;  
 $\max_{ij}$  = maximum value of  $i$ th coordinate,  $j$ th hypervolume.

Let us consider an example of application using equation (V-2). Suppose that we have a system with  $n = 3$  and examine a single hypervolume with the following coordinate ranges:

coordinate	min value	max value
1	0	2
2	0	3
3	1	2

The hypervolume contains 24 points. If we use only the binomial coefficients as shorthand representation for complete terms, then by (V-1)

$$\sum_{A \in HV_j} \prod_{i=1}^3 \binom{m_i}{a_i} = \binom{m_1}{0^1} \binom{m_2}{0^2} \binom{m_3}{1^3} + \dots + \binom{m_1}{2^1} \binom{m_2}{3^2} \binom{m_3}{2^3}, \quad (V-3)$$

whereas the representation for (V-2) would be

$$\prod_{i=1}^3 \sum_{k=\min_{ij}}^{\max_{ij}} \binom{m_i}{k} = \left[ \binom{m_1}{0^1} + \binom{m_1}{1^1} + \binom{m_1}{2^1} \right] \left[ \binom{m_2}{0^2} + \binom{m_2}{1^2} + \binom{m_2}{2^2} + \binom{m_2}{3^2} \right] \left[ \binom{m_3}{1^3} + \binom{m_3}{2^3} \right]. \quad (V-4)$$

The arithmetic operations to be made in each of these equations are summarized in Table I.

Table I

Type of Operation	Number of Operations Necessary	
	Equation (V-3)	Equation (V-4)
Exponentiation	144	18
Multiplication	192	20
Addition	23	6

A similar but somewhat more involved factorization of equation (IV-16) can also be made. In terms of summation over hypervolumes (IV-16) becomes

$$B = \sum_{j=1}^M \left\{ \sum_{A_eHV_j} \left( \prod_{i=1}^n p_i \right) \left( \sum_{i=1}^n c_i \right) \right\}. \quad (V-5)$$

Over any single hypervolume,  $HV_j$ , we can rewrite the summations and products so that

$$\sum_{A \in HV_j} \left\{ \prod_{i=1}^n \binom{m_i}{a_i} p_i^{a_i} (1-p_i)^{m_i - a_i} \right\} \left\{ \sum_{i=1}^n \frac{a_i - m_i p_i}{1 - p_i} \right\}$$

$$= \sum_{l=1}^n \left\{ \prod_{i=1}^n \left[ \sum_{k=\min_{i,j}}^{\max_{i,j}} \binom{m_i}{k} p_i^k (1-p_i)^{m_i - k} \delta_{il} \right] \right\} \quad (V-6)$$

where  $\min_{i,j}$  = minimum value of ith coordinate, jth hypervolume;

$\max_{i,j}$  = maximum value of ith coordinate, jth hypervolume;

and

$$\delta_{il} = \begin{cases} 1 & \text{if } i \neq l \\ \frac{k - m_i p_i}{1 - p_i} & \text{if } i = l. \end{cases} \quad (V-7)$$

Note that in (V-6) and (V-7) the function  $\delta_{il}$  has no relation whatsoever to the step size  $\delta$  used earlier in the discussion. The step function  $\delta_{il}$  is necessary in (V-6), since we are concerned with a product/sum combination over hypervolumes rather than a product-only operation. Equation (V-6) has the feature of being able to use the hypervolume information available without intermediate steps of hypervolume component rearrangement necessary for equation (V-5).



The most illustrative, nontrivial example for comparing (V-6) with (V-5) is a two-dimensional system where the hypervolume coordinate minimums and maximum have the following values:

coordinate	min value	max value
1	0	2
2	0	1

Let  $c_{ik} = \frac{k - m_i p_i}{1 - p_i}$  and

$\binom{m_i}{k}$  represent  $\binom{m_i}{k} p_i^k (1 - p_i)^{m_i - k}$ .

Then by (V-5),

$$\sum_{A \in HV_j} \left( \prod_{i=1}^2 b_i \right) \left( \sum_{i=1}^2 c_i \right) =$$

$$\left\{ \begin{array}{l} \binom{m_1}{0^1} \binom{m_2}{0^2} [c_{10} + c_{20}] + \binom{m_1}{0^1} \binom{m_2}{1^2} [c_{10} + c_{21}] + \\ \binom{m_1}{1^1} \binom{m_2}{0^2} [c_{11} + c_{20}] + \binom{m_1}{1^1} \binom{m_2}{1^2} [c_{11} + c_{21}] + \\ \binom{m_1}{2^1} \binom{m_2}{0^2} [c_{12} + c_{20}] + \binom{m_1}{2^1} \binom{m_2}{1^2} [c_{12} + c_{21}] \end{array} \right\} \quad (V-8)$$

From (V-6),

$$\sum_{\ell=1}^2 \left\{ \prod_{i=1}^2 \left[ \sum_{k=\min_{ij}}^{\max_{ij}} \binom{m_i}{k} \delta_{i\ell} \right] \right\} =$$

$$\left\{ \begin{aligned} & \left[ \binom{m_1}{0} c_{10} + \binom{m_1}{1} c_{11} + \binom{m_1}{2} c_{12} \right] \left[ \binom{m_2}{0} + \binom{m_2}{1} \right] + \\ & \left[ \binom{m_1}{0} + \binom{m_1}{1} + \binom{m_1}{2} \right] \left[ \binom{m_2}{0} c_{20} + \binom{m_2}{1} c_{21} \right] \end{aligned} \right\} \quad (V-9)$$

Equations (V-8) and (V-9) can be shown to be comparable by collecting like terms in each.

Assuming the  $c_{ik}$  terms can be evaluated once and then inserted in the equations wherever needed, we summarize the number of operations necessary to complete (V-8) and (V-9) in Table II.

Table II

Type of Operation	Number of Operations Necessary	
	Equation (V-8)	Equation (V-9)
Exponentiation	24	20
Multiplication	36	27
Addition	11	7

Without writing the expansions, we find the number of operations necessary to evaluate (V-5) and (V-6) for the first example summarized in Table III.

Table III

Type of Operation	Number of Operations Necessary	
	Equation (V-5)	Equation(V-6)
Exponentiation	144	54
Multiplication	216	69
Addition	71	20

In all of these equations, some of the operations can be avoided by storing similar terms for repeated use. This is particularly true for the exponentiations that must be performed. But clearly, for larger hypervolumes and larger systems the chasm between the number of operations necessary to evaluate (V-2) and (V-6) as opposed to (V-1) and (V-5) increases substantially.

Computationally, the evaluation of the binomial coefficients can be accelerated by

- (1) selecting some integer  $N$ , computing  $n!$  once for each integer  $n = 1, \dots, N$ , and storing these factorials in an array for ready access whenever needed;
- (2) approximating the binomial coefficient involving integers greater than  $N$ .

The value of N chosen is dependent primarily on the exponent range of the computer being used. Of secondary consideration is the size of the integers to be encountered in most problems; i.e., the number of component tests that will normally be made and the size of N covering most values. Rewriting the binomial coefficient in terms of gamma functions, we have

$$\binom{n}{r} = \frac{n!}{r!(n-r)!} = \frac{\Gamma(n+1)}{\Gamma(r+1)\Gamma(n-r+1)} \quad (V-10)$$

Stirling's formula [5] for an approximation to the logarithm of the gamma function is

$$\ln \Gamma(n) \sim (n - \frac{1}{2}) \ln n - n + \frac{1}{2} \ln 2\pi + \frac{1}{12n} \quad (V-11)$$

Using the logarithmic form (V-11) in (V-10), we find

$$\begin{aligned} \ln \binom{n}{r} &= n \ln \left( \frac{n+1}{n-r+1} \right) + r \ln \left( \frac{n-r+1}{r+1} \right) + \frac{1}{2} \ln \left\{ \frac{n+1}{(r+1)(n-r+1)} \right\} \\ &+ (1 - \frac{1}{2} \ln 2\pi) + \frac{r(n-r) - (n+1)^2}{12(n+1)(r+1)(n-r+1)} \quad (V-12) \end{aligned}$$

Combining the numerator and denominator terms of (V-10) into a single operation prevents exponent overflow that might occur should each term be evaluated separately and then a division be attempted. This is particularly true in the situation where the value of  $N$  has been selected to permit as great an exponent range as possible for calculating  $N!$ .

In some problems it may be that the initial starting point  $\bar{P}$  is so far above the constraint curve  $H$ ,  $H(\bar{P}) \ll 1 - \alpha$ , that the first-order approximation (IV-20) cannot provide a sufficient  $\Delta p$  correction to even place the next point in the vicinity of the constraint curve. This condition can be likened to one of trying to determine the root of an equation through the Newton-Raphson method. It is well known that should a poor initial guess be used in starting the iteration, the method can place the next step completely away from the root to be found. The first-order approximation in (IV-20) reacts in a very similar manner. Fig. 8 illustrates the situation that can arise.

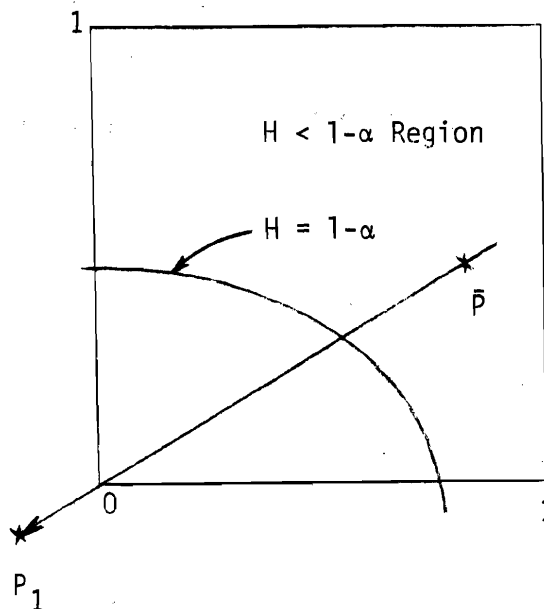


Figure 8

The proposed improvement places the point  $P_1$  in violation of the boundary conditions imposed upon the variables.

By eliminating the higher orders from the approximation to simplify the resulting equation (IV-12), the contribution necessary from the higher ordered terms to prevent "overshoot" was also eliminated. Hence, approximations involving second- and third-ordered terms were derived to examine what improvement could be made. In light of the tremendous number of calculations needed to evaluate these approximations and after some preliminary trials of use, it was decided that although improvement of the approximation could be made the time involved to do so was prohibitive on any problems beyond the very simple.

Guided from experience in the problems of root-finding, we chose to use a method of bisection in moving to a more advantageous starting point. We know from the nature of this problem that the initial point falls in the vicinity of a maximum  $f$  value but for some other constraint curve. Because the constraint curves have relatively similar characteristics of behavior and do not intersect, we sought a more reasonable starting point along a line connecting the initial point supplied and the origin.

Let us define

$$\begin{aligned}\Delta_0 &= H(0) - (1 - \alpha) > 0 , \\ \Delta_1 &= H(\bar{P}) - (1 - \alpha) < 0 , \\ \Delta_j &= H(P_j) - (1 - \alpha) \text{ for } j \geq 2 .\end{aligned}\tag{V-13}$$

We consider the sequence of points which lie halfway between the previous two points producing  $\Delta$  values from (V-13) of opposite signs. The sequence is described by the equations

$$P_{j+1} = P_j - \frac{1}{2} (P_j - P_{j-1}) \text{ for } \Delta_{j-1} > 0, \Delta_j < 0; \quad (\text{V-14})$$

$$P_{j+1} = P_j + \frac{1}{2} (P_{j-1} - P_j) \text{ for } \Delta_{j-1} < 0, \Delta_j > 0. \quad (\text{V-15})$$

Each step requires that a new H function be evaluated and in our previous discussion we have seen that this can become time consuming. Hence, bisection is continued via (V-14) and (V-15) only until a point is found within a region of the constraint curve for which the more expedient approximation can be used. The criterion established for choosing a stopping point  $P_{j+1}$  is when

$$|\Delta_{j+1}| \leq \frac{1}{2}(1 - \alpha). \quad (\text{V-16})$$

Since the method and the equations utilized to obtain a maximum value for function under the prescribed constraints have been described, the entire procedure is reduced to algorithmic form in the following section.

## VI. Algorithm for Nonlinear Function Maximization

This algorithm assumes prior construction of the index set  $\psi$  in terms of hypervolumes, as detailed in Section III, necessary for evaluation of various equations presented in Section V.

1. Determine the initial starting point  $\bar{P} = (\bar{p}_1, \bar{p}_2, \dots, \bar{p}_n)$  by Equation (IV-2) and calculate the corresponding function value  $H(\bar{P})$  as expressed in Equation (V-2).
2. From Equation (V-5) calculate the value of  $B$  which, when substituted into (IV-20) together with  $H(\bar{P})$ , will provide the necessary  $\Delta p$  shift value to yield the first point  $P_I$  on or near the constraint curve (Ref. Figure 4). Determine  $H(P_I)$  by Equation (V-2).
3. Test the validity of the values  $(p_1, p_2, \dots, p_n)_I$ . If  $0 < p_k < 1$  for all  $k, k=1, \dots, n$ , we have an acceptable point on the constraint curve. Go to step 5.

If  $p_k \leq 0$  or  $p_k \geq 1$  for any  $k, k=1, \dots, n$ , then the initial starting point  $\bar{P}$  was too far removed from the constraint curve and we would overshoot the problem boundary conditions. A more reasonable starting point must be found. Go to step 4.

4. For the method of bisection, determine a new starting point  $\bar{P}$  by using Equations (V-13, 14, 15). Repeat the calculations of steps 2-4 until the criterion of acceptance for the bisection (V-16) has been met. Determine the point  $P_I$  on or near the constraint curve as described in step 2 and, upon completion, proceed on to step 5.
5. Calculate the intersecting function value  $f_I$ . Thus, the envelope of enclosure for the next point  $\hat{P}_I$  has been formed. Also determine the initial increment values  $\delta_s$  and  $\delta_p$  for series and parallel components, respectively. (Let the generic term  $\delta$  represent either  $\delta_s$  or  $\delta_p$  according to the component application). Go to step 6.



6. Determine the series component to be selected to serve as the slack component for the current step cycle. If specific branch paths are dictated as a result of a detected oscillation, slack component has been fixed so go to 7. For no oscillation yet detected, go on to 6a.
  - (a). Check step movement. If oscillation is taking place, go to 6b. If no oscillation, go to 7.
  - (b). For oscillation between components, test sufficiency condition (IV-21). Go to 7 if sufficient progress. Otherwise, a junction exists and if user indicates a continuation of maximization, go to 6c. If user indicates a halt at a junction, print out diagnostic message with all pertinent information.
  - (c). For maximization along several branches, flag all slack components involved in the oscillation as separate branch paths to be followed. Also save junction point data for the restart of each path.
7. Define  $\hat{p}_{n-1} = p_{n-1} + \delta$ .
  - (a). If  $\hat{p}_{n-1} < 1$ , continue to 7b. Otherwise,  $\hat{p}_{n-1} \geq 1$ , which violates the boundary restrictions. In this case, go to step 8.
  - (b). The slack component,  $\hat{p}_n$ , is defined by Equation (IV-4) to maintain a position on the  $f_I$  curve. Thus,  $\hat{P}_I = (p_1, \dots, p_{n-2}, \hat{p}_{n-1}, \hat{p}_n)$ . If  $H(\hat{P}_I) \geq H(P_I)$ , go to step 10. Otherwise, the point  $\hat{P}_I$  has been moved beyond the envelope and we go to step 8.
8. Try the opposite direction. Define  $\hat{p}_{n-1} = p_{n-1} - \delta$ .
  - (a). If  $\hat{p}_{n-1} > 0$ , continue to 8b. Otherwise,  $\hat{p}_{n-1} \leq 0$ , which also violates the boundary restrictions. In this case, go to step 9.

- (b). Follow the same procedure as step 7b to determine  $\hat{p}_n$ . If  $H(\hat{P}_I) \geq H(P_I)$ , go to step 10. If not, then  $\hat{P}_I$  is outside the envelope and we go to step 9.
9. The component  $p_{n-1}$  could not be incremented or decremented with the currently fixed step size  $\delta$ . Define  $\hat{p}_{n-1} = p_{n-1}$  and  $\hat{p}_n = p_n$ . Proceed to step 10.
10. Looping on  $i, i=n-2, \dots, 1$ , modify each component  $p_i$  by  $\delta$  in the manner described in steps 7 and 8 and in Equation (IV-5). Upon completion, the final point position  $\hat{P}_I$  has been determined.
- (a). If any of the components,  $p_i$ , were modified by  $\delta$  then calculate  $H(\hat{P}_I)$  and go to 12.
- (b). If it was not possible to modify any component  $p_i, i=1, \dots, n-1$ , by  $\delta$  and stay within the criteria of movement, a smaller step size must be used. Go to step 11.
11. Reduce the step size,  $\delta_s^1 = \delta_s / 2, \delta_p^1 = \sqrt{\delta_s^1}$ . Return to step 7.
12. As described in step 2, use Equations (IV-20) and (V-5) to calculate the necessary values to produce the next point on the constraint curve. Go on to 13.
13. Follow the same procedure as detailed in steps 6 through 10 to determine the next point  $\hat{P}_j$ . Provided that the criteria placed upon  $\hat{P}_j$  are satisfied ( $H(\hat{P}_j) \geq H(P_j)$  and boundary conditions met), return to step 12 to determine  $P_{j+1}$ . Thus begins an iterative procedure,  $j=1, 2, \dots, M$ , in locating the maximum value for the function  $f$ . If it was not possible to modify any of the components of  $P_j$  without violating a part of the criteria, go to step 14.

14. The  $\delta$  step size was too large for the current envelope of containment and must be reduced,  $\delta_s^{k+1} = \delta_s^k/2$  and  $\delta_p^{k+1} = \sqrt{\delta_s^{k+1}}$ .

With some number of decimal places,  $d$ , of accuracy prescribed for the series components, check  $\delta_s^{k+1}$ .

(a). If  $\delta_s^{k+1} \geq 10^{-d}$ , go to step 13.

(b). If  $\delta_s^{k+1} < 10^{-d}$ , go to step 15.

15. Convergence criterion has been met and the final point  $P^* = (p_1^*, \dots, p_n^*) = (p_1, \dots, p_n)_M$  established so that

$$f(P^*) = \text{Max}_{j=1}^M f(P_j) ; H(P^*) = 1-\alpha.$$

16. Test on branch paths.

(a). If no oscillation is indicated, maximization procedure has been completed as described in step 15.

(b). If oscillation is indicated, branch paths are being taken. If all branch paths are exhausted, maximization procedure is completed. Otherwise, return to step 7 with a new fixed slack component for a new path to be followed.

## VII. Conclusions

The material presented in this report is not the last word in efforts to arrive at new ideas and methods of solution for the problem posed: confidence limits for system failure probability. Certainly, major progress has been made by taking a theoretical equation with seemingly unfathomable computational roadblocks into the realm of real-life application.

Methods of checking the hypervolume construction have been described in Section III. Summaries of the various systems considered in testing the methods proposed are presented in the appendices, along with system diagrams, initial parameters, resultant failure probabilities at different confidence levels, the size of related index sets, and the amount of computer time needed for solutions. These test systems not only serve as the "shake-down" of the computer code, CONLIM, but also indicate the nature of problems that can be analyzed and the directions for usage of CONLIM.

As described by Wilde [6], one of the principal indicators of preferred optimization occurs in the greatest possible interval of uncertainty to obtain the maximum value sought. Furthermore, a sequential search using previously discovered information can greatly assist in the search process of maximization. By enclosing the interval of search within the boundary envelopes described in Section IV, we actually utilize a sequential process in each successive step, and as a result, the interval of uncertainty for maximization is narrowed with each step.

Several factors appear to be critical when a system for analysis is considered. None can be considered independently, but must be viewed in conjunction with each of the other factors. All are an integral part of the system complexity. The first and most obvious factor is the size of

the system and the number of unique components making up the system. Not only does the index set increase in size and scope, thus requiring a longer construction period, but the maximization procedure also must take into consideration more variables to be examined. The conditions of iteration and convergence apply to all components and thus the time for solution to the problem becomes lengthened.

Secondly, the arrangement of components can be a factor in the amount of time required for a solution. We have observed that systems containing many series-connected components require more time for solution, as opposed to systems made up of several parallel combinations.

Another factor must be considered in relation to the arrangement scheme and the dimension of the system. Parameters input to the problem include the number of failures  $x_i$ ,  $i=1, \dots, n$ , that were found in  $m_i$ ,  $i=1, \dots, n$ , tests performed on each component. In the case of a series component and, to a lesser degree, of a parallel component, the higher the failure rate the more critical that component becomes to the system. The function criterion for hypervolume acceptance enlarges as the ratio  $x_i/m_i$  increases for any  $i$ th component. This means a larger space under the surface to be filled by hypervolumes; the greater the number of hypervolumes, the greater the amount of computation to be done in evaluating the various maximization equations.

Of course the amount of time required for the computation of predicted failure probability should be considered. Only in special cases would an expected poor system even be considered for use. We must hold as the final criteria for using any technique the importance of the system and the accuracy of prediction desired. In those instances where a question of the global maximum arises as a result of branch paths, we clearly indicate the possible choices available without hesitation.

The use of hypervolume construction for the index sets and the method presented for function maximization open the door for analysis of systems ranging from the most simple composition to those of a complex, many-component structure. We cannot overemphasize the possibilities of application to the myriad of differing types of systems. Aside from the application to new systems under consideration, this approach permits a standard of comparison for previously used or proposed approximations of failure probability analysis.

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## APPENDIX A

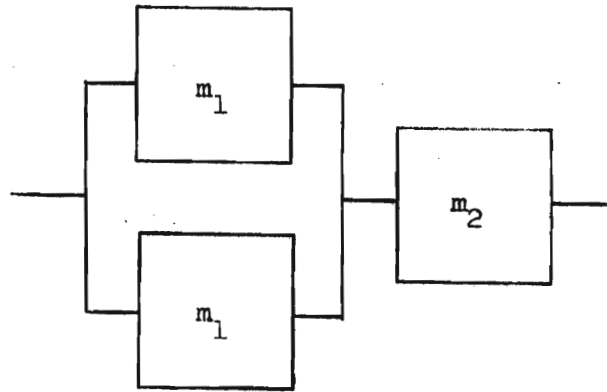
### SYSTEMS UTILIZED TO STUDY AND TEST CONLIM

Diagrams for each of the test systems are given in this appendix. In many of the tests, several different input parameters are provided for comparison checks on resultant values. The probability functions,  $f$ , describing each system are also provided.

The appendices following are related to this appendix via the identification of system number and test number subordinate to each system.



SYSTEM 1 (2-D)



$$f = p_1^2 + p_2 (1 - p_1^2)$$

Test 1

$$m_1 = 20, x_1 = 1$$

$$m_2 = 20, x_2 = 1$$

Test 2

$$m_1 = 40, x_1 = 1$$

$$m_2 = 40, x_2 = 1$$

Test 3

$$m_1 = 40, x_1 = 2$$

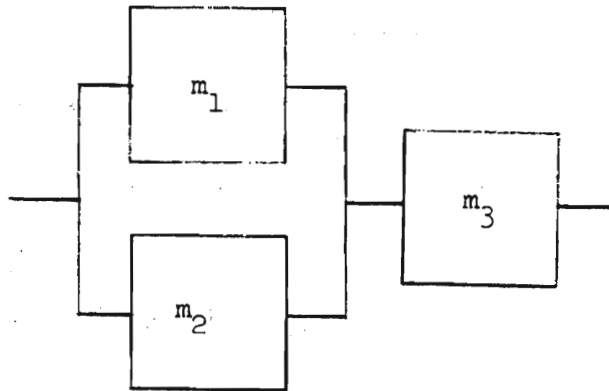
$$m_2 = 40, x_2 = 2$$

Test 4

$$m_1 = 40, x_1 = 3$$

$$m_2 = 40, x_2 = 3$$

SYSTEM 2 (3-D)



$$f = p_1 p_2 + p_3 (1 - p_1 p_2)$$

Test 1

$$m_1 = 20, x_1 = 1$$

$$m_2 = 20, x_2 = 1$$

$$m_3 = 20, x_3 = 1$$

Test 2

$$m_1 = 40, x_1 = 2$$

$$m_2 = 40, x_2 = 2$$

$$m_3 = 40, x_3 = 2$$

Test 3

$$m_1 = 40, x_1 = 4$$

$$m_2 = 40, x_2 = 9$$

$$m_3 = 40, x_3 = 1$$

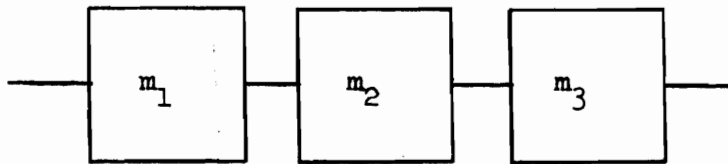
Test 4

$$m_1 = 40, x_1 = 2$$

$$m_2 = 40, x_2 = 20$$

$$m_3 = 40, x_3 = 0$$

SYSTEM 3 (3-D)



$$f = 1 - (1 - p_1)(1 - p_2)(1 - p_3)$$

$$\sim p_1 + p_2 + p_3$$

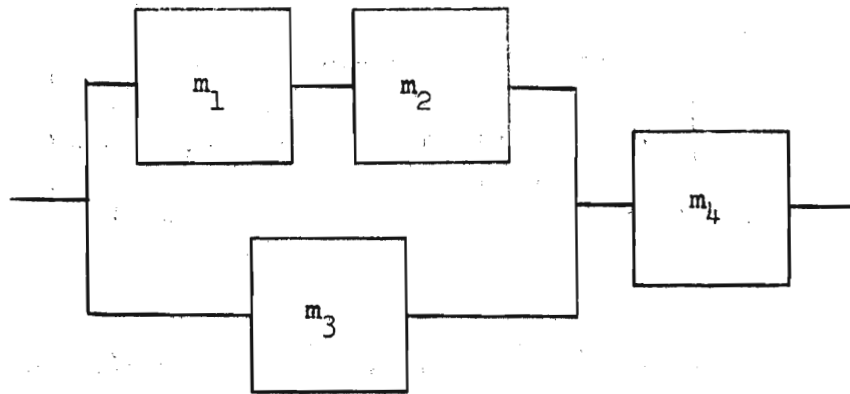
Test 1

$$m_1 = 20, x_1 = 1$$

$$m_2 = 15, x_2 = 0$$

$$m_3 = 10, x_3 = 0$$

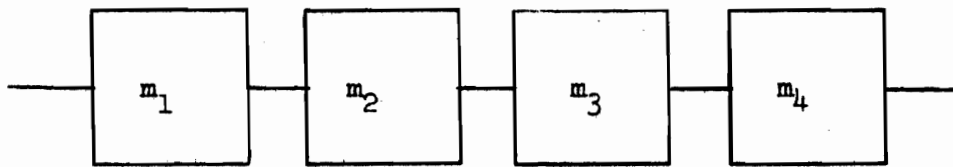
SYSTEM 4 (4-D)



$$f = 1 - (1 - p_4) [1 - p_3 (p_1 + p_2 - p_1 p_2)]$$

<u>Test 1</u>	<u>Test 2</u>	<u>Test 3</u>
$m_1 = 30, x_1 = 1$	$m_1 = 20, x_1 = 1$	$m_1 = 40, x_1 = 2$
$m_2 = 20, x_2 = 1$	$m_2 = 30, x_2 = 1$	$m_2 = 60, x_2 = 2$
$m_3 = 25, x_3 = 1$	$m_3 = 25, x_3 = 1$	$m_3 = 50, x_3 = 2$
$m_4 = 20, x_4 = 1$	$m_4 = 20, x_4 = 1$	$m_4 = 40, x_4 = 2$

SYSTEM 5 (4-D)



$$f = 1 - [(1 - p_1)(1 - p_2)(1 - p_3)(1 - p_4)]$$

Test 1

$$m_1 = 49, x_1 = 0$$

$$m_2 = 41, x_2 = 1$$

$$m_3 = 23, x_3 = 0$$

$$m_4 = 48, x_4 = 5$$

Test 2

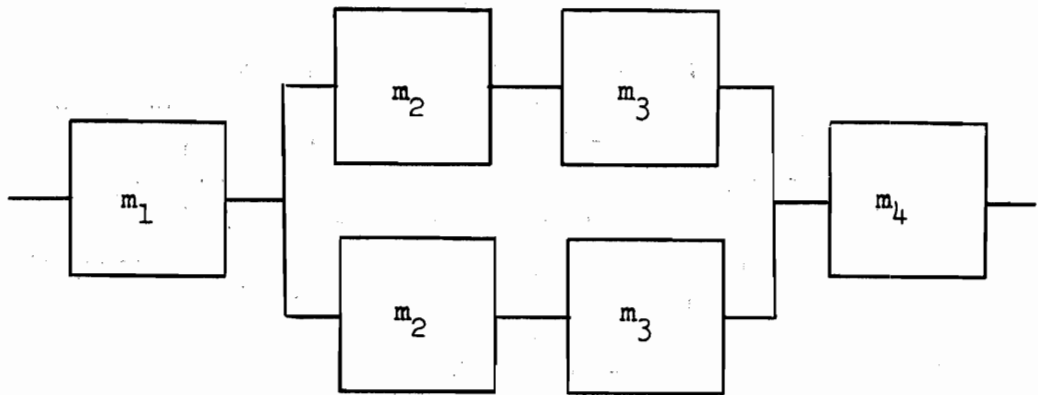
$$m_1 = 48, x_1 = 5$$

$$m_2 = 41, x_2 = 1$$

$$m_3 = 23, x_3 = 0$$

$$m_4 = 49, x_4 = 0$$

SYSTEM 6 (4-D)

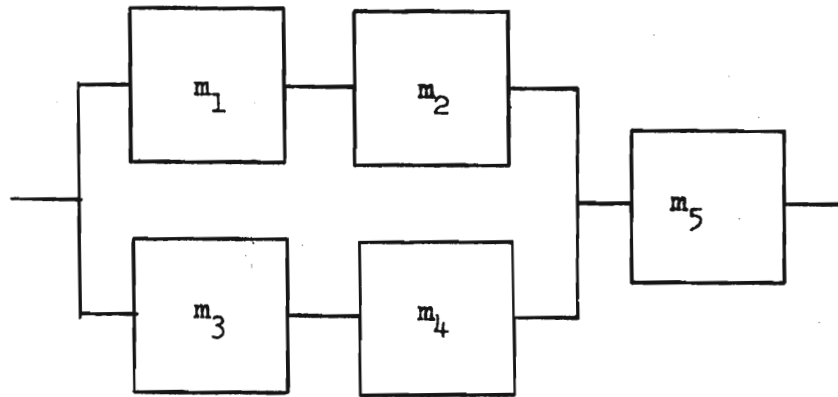


$$f = p_4 + (1 - p_4) f'$$

$$f' = p_1 + (1 - p_1) [p_2 + (1 - p_2) p_3]^2$$

<u>Test 1</u>	<u>Test 2</u>	<u>Test 3</u>
$m_1 = 40, x_1 = 1$	$m_1 = 40, x_1 = 1$	$m_1 = 40, x_1 = 0$
$m_2 = 50, x_2 = 2$	$m_2 = 50, x_2 = 1$	$m_2 = 50, x_2 = 0$
$m_3 = 50, x_3 = 1$	$m_3 = 50, x_3 = 2$	$m_3 = 50, x_3 = 0$
$m_4 = 20, x_4 = 0$	$m_4 = 20, x_4 = 0$	$m_4 = 20, x_4 = 0$

SYSTEM 7 (5-D)



$$f = p_5 + (1 - p_5) \left[ p_1 + (1 - p_1) p_2 \right] \left[ p_3 + (1 - p_3) p_4 \right]$$

Test 1

$$m_1 = 30, x_1 = 2$$

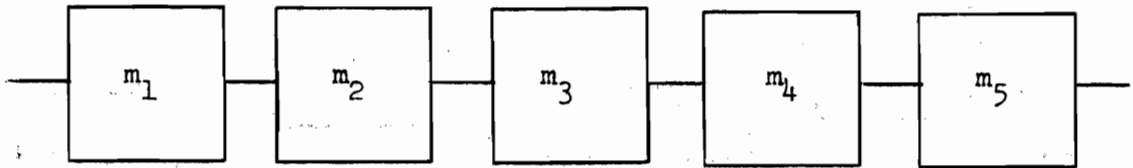
$$m_2 = 20, x_2 = 1$$

$$m_3 = 40, x_3 = 2$$

$$m_4 = 30, x_4 = 1$$

$$m_5 = 20, x_5 = 1$$

SYSTEM 8 (5-D)



$$f = 1 - (1 - p_1)(1 - p_2)(1 - p_3)(1 - p_4)(1 - p_5)$$

Test 1

$$m_1 = 50, x_1 = 0$$

$$m_2 = 50, x_2 = 0$$

$$m_3 = 50, x_3 = 0$$

$$m_4 = 50, x_4 = 0$$

$$m_5 = 50, x_5 = 1$$

Test 2

$$m_1 = 50, x_1 = 1$$

$$m_2 = 50, x_2 = 0$$

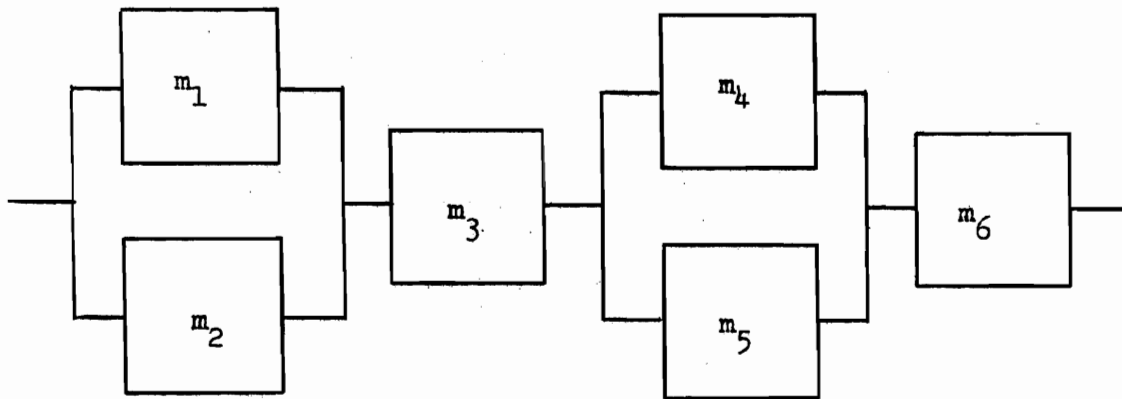
$$m_3 = 50, x_3 = 0$$

$$m_4 = 50, x_4 = 0$$

$$m_5 = 50, x_5 = 0$$



SYSTEM 9 (6-D)



$$f = 1 - [(1 - p_1 p_2)(1 - p_4 p_5)(1 - p_3)(1 - p_6)]$$

Test 1

$$m_1 = 20, x_1 = 1$$

$$m_2 = 25, x_2 = 0$$

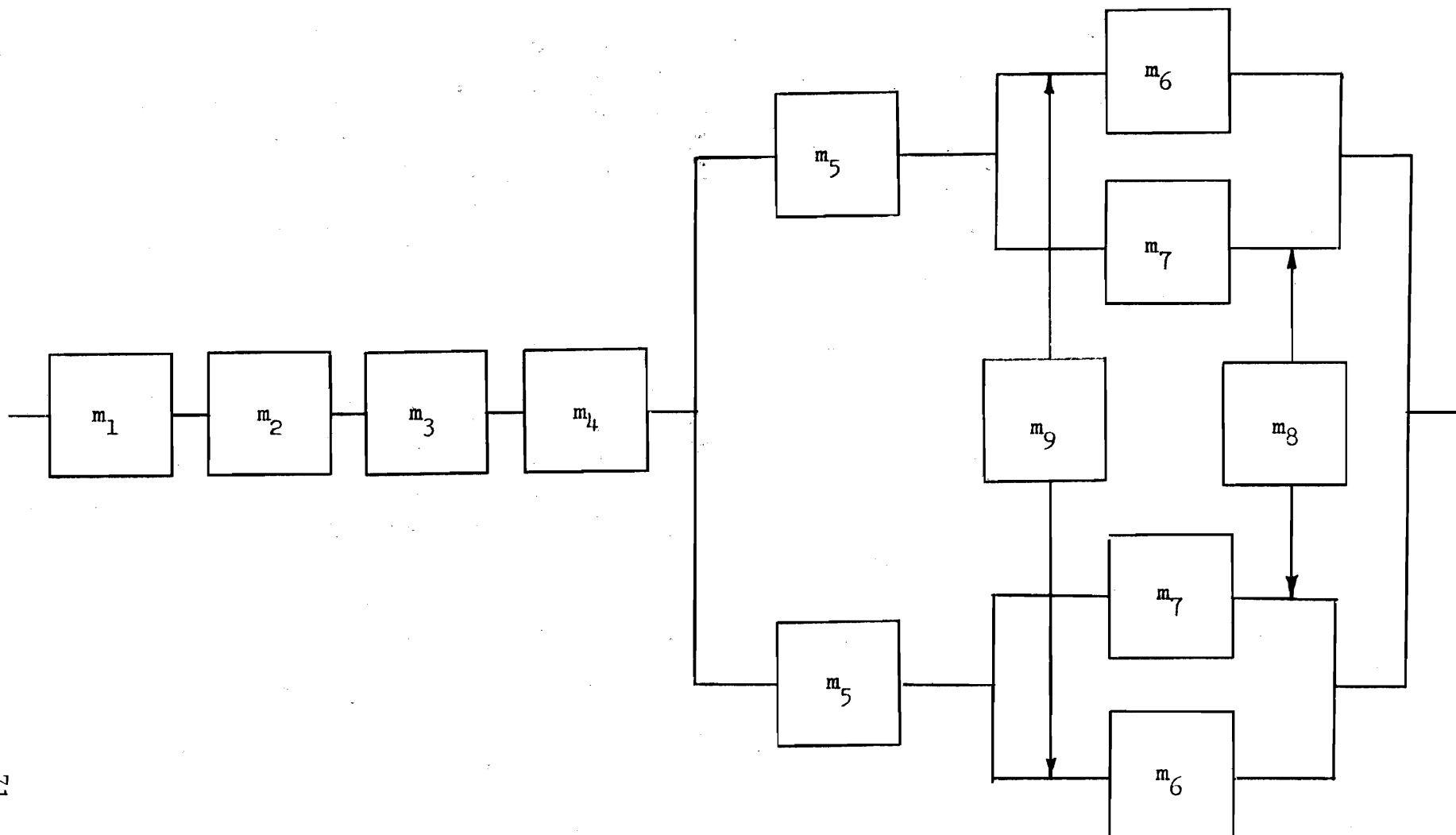
$$m_3 = 30, x_3 = 1$$

$$m_4 = 25, x_4 = 1$$

$$m_5 = 20, x_5 = 1$$

$$m_6 = 40, x_6 = 0$$

SYSTEM 10 (9-D)



SYSTEM 10  
(CONTINUED)

$$\begin{aligned}
 f = 1 - \prod_{i=1}^4 (1 - p_i) & \left[ (1 - p_9)(1 - p_8) \left\{ 1 - \left( 1 - [1 - p_5][1 - p_6 p_7] \right)^2 \right\} \right. \\
 & + p_9 (1 - p_8) \left\{ 1 - \left( p_5 + [1 - p_5] p_7 \right)^2 \right\} \\
 & \left. + p_8 (1 - p_9) \left\{ 1 - \left( p_5 + [1 - p_5] p_6 \right)^2 \right\} \right]
 \end{aligned}$$

<u>Test 1</u>	<u>Test 2</u>	<u>Test 3</u>	<u>Test 4</u>
$m_1 = 44, x_1 = 0$	$m_1 = 44, x_1 = 0$	$m_1 = 44, x_1 = 0$	$m_1 = 44, x_1 = 0$
$m_2 = 54, x_2 = 0$	$m_2 = 54, x_2 = 0$	$m_2 = 54, x_2 = 0$	$m_2 = 54, x_2 = 1$
$m_3 = 30, x_3 = 0$	$m_3 = 30, x_3 = 0$	$m_3 = 30, x_3 = 0$	$m_3 = 30, x_3 = 0$
$m_4 = 101, x_4 = 0$	$m_4 = 101, x_4 = 1$	$m_4 = 101, x_4 = 0$	$m_4 = 101, x_4 = 0$
$m_5 = 32, x_5 = 1$	$m_5 = 32, x_5 = 1$	$m_5 = 32, x_5 = 2$	$m_5 = 32, x_5 = 1$
$m_6 = 23, x_6 = 1$	$m_6 = 23, x_6 = 1$	$m_6 = 23, x_6 = 3$	$m_6 = 23, x_6 = 1$
$m_7 = 32, x_7 = 1$	$m_7 = 32, x_7 = 1$	$m_7 = 32, x_7 = 2$	$m_7 = 32, x_7 = 1$
$m_8 = 43, x_8 = 1$	$m_8 = 43, x_8 = 1$	$m_8 = 43, x_8 = 3$	$m_8 = 43, x_8 = 1$
$m_9 = 17, x_9 = 0$	$m_9 = 17, x_9 = 0$	$m_9 = 17, x_9 = 0$	$m_9 = 17, x_9 = 0$

APPENDIX B

INDEX SET COMPOSITION AND CONSTRUCTION TIME  
OF CONLIM TEST SYSTEMS

Index Set Composition and Construction Time

System	Test	Index Set $\Psi$		
		No. of HV	No. of n-tuples	time (secs.)
1	1	2	7	0.001
	2	2	8	0.001
	3	3	19	0.002
	4	4	32	0.003
2	1	12	89	0.009
	2	34	543	0.041
	3	33	524	0.040
	4	22	295	0.023
3	1	1	2	0.001
4	1	65	1243	0.107
	2	69	1243	0.115
	3	414	15404	2.42
5	1	39	109	0.045
	2	39	109	0.043
6	1	10	44	0.010
	2	10	44	0.009
	3	1	1	0.001
7	1	583	6061	6.88
8	1	5	6	0.004
	2	5	6	0.004
9	1	373	2848	2.52
10	1	44	183	0.38
	2	433	2451	11.5
	3	675	3726	23.2
	4	1665	8912	119.3

APPENDIX C

CONLIM RESULTS OF SYSTEM TESTS

System	Test	$\alpha=0.80$		$\alpha=0.90$		$\alpha=0.95$		$\alpha=0.98$		$\alpha=0.99$	
		f value	time	f value	time	f value	time	f value	time	f value	time
1	1	0.14226	0.02	0.18095	0.03	0.21606	0.03	0.25878	0.03	0.28820	0.03
	2	0.07288	0.02	0.09378	0.03	0.11311	0.03	0.13733	0.03	0.15104	0.02
	3	0.10382	0.05	0.12763	0.06	0.14915	0.07	0.17540	0.06	0.19401	0.06
	4	0.13372	0.12	0.15960	0.11	0.18273	0.12	0.21054	0.15	0.23004	0.14
2	1	0.14243	0.33	0.18095	0.34	0.21602	0.34	0.25177	0.32	0.28877	0.39
	2	0.10402	1.68	0.12769	1.82	0.14921	1.95	0.17546	2.36	0.19406	2.18
	3	0.10397	2.36	0.12764	1.97	0.14916	2.15	0.17541	2.20	0.19402	2.36
	4	0.07427	2.11	0.09503	2.09	0.11439	2.12	0.13851	2.31	0.15588	2.33
3	1	0.17026	0.03	0.22809	0.03	0.26451	0.03	0.33026	0.03	0.37584	0.03
4	1	0.14243	3.80	0.18096	6.47	0.21611	6.27	0.25879	4.66	0.28879	4.84
	2	0.14243	3.64	0.18096	6.41	0.21611	6.26	0.25879	4.27	0.28879	4.66
	3	0.10412	63.5	0.12779	44.1	0.14931	60.7	0.17555	61.7	0.19416	63.2
5	1	0.19772	6.32	0.23480	6.26	0.26793	6.77	0.30750	6.92	0.33500	8.18
	2	0.19772	5.79	0.23480	5.97	0.26793	6.32	0.30750	6.50	0.33500	7.84
6	1	0.08120	1.37	0.11760	2.58	0.14272	0.94	0.18111	1.01	0.21357	1.45
	2	0.08120	1.40	0.11760	2.56	0.14272	1.08	0.18111	1.06	0.21357	1.46
	3	0.07419	0.07	0.10719	0.08	0.13668	0.08	0.17280	0.07	0.20488	0.09
7	1	0.14316	89.9	0.18165	87.7	0.21677	81.5	0.25941	78.5	0.28939	72.7
8	1	0.05870	0.83	0.07558	0.79	0.09140	0.93	0.11119	0.88	0.12552	0.90
	2	0.05870	0.83	0.07558	0.79	0.09140	0.92	0.11119	0.87	0.12552	0.90
9	1	0.09655	64.3	0.12357	63.1	0.14860	64.4	0.17950	64.4	0.20159	81.4
10	1	0.05221	12.1	0.07388	13.1	0.09503	13.4	0.12226	14.8	0.14230	13.9
	2	0.05400	197.5	0.07561	236.9	0.09672	210.0	0.12390	194.8	0.14391	224.3
	3	0.05418	348.6	0.07578	365.1	0.09689	399.1	0.12407	639.4	0.14407	728.5
	4	0.05972	1789								

NOTE: All times shown are in seconds

## APPENDIX D

### EXAMPLES OF INPUT DATA AND CONTROL CARDS FOR CONLIM

The specific data input structure for CONLIM is detailed on the first two pages of Appendix F in the computer code listing of CONLIM. Each data card is described, and the particular format arrangement for each card is also provided. Users of CONLIM are directed to those two pages for references, as well as to the sample decks listed in this appendix.

We note that for systems of dimension greater than 8, the user must perform a minor modification to CONLIM. Two cards, CONLIM 117 and CONLIM 118, must be replaced since the limiting dimension automatically accommodated by CONLIM is set at 8. The reason for this dimension value is only to maintain CONLIM at a computer memory core requirement less than 100,000<sub>8</sub> words and in no way reflects upon the capabilities of CONLIM. The card deck structure from one of the sample tests described in the preceding appendices (System 10) is presented in this appendix to demonstrate the necessary modifications.

In addition to the numerical input data, the user also has the responsibility of supplying the function QTHETA (PROB), which describes the reliability function of the system under study. PROB is an array which must be dimensioned N, the size of the system. Examples of such functions are included on the following pages. Both QTHETA and PROB are probabilities in terms of system failure and component failure, respectively.



```

SYSTEM1,T---,CM100000,EC---.
ACCOUNT,S-----,D-----,G-----,A-----,R-,K---.
ATTACH,CONTAP,CONLIM.
COPYBF,CONTAP,LGO.
FTN,B=LGO1,L,OPT=1.
REWIND,LGO1.
PREP,LGO1,QTHE.
COLLCT,LGO,FTNLIB,QTHE.
LGO.
7/8/9

```

IDENTIFICATION

In this example, the program CONLIM resides in a permanent file in binary form. The function deck is compiled and collected to the program for execution.

```

FUNCTION QTHETA(PROB)

```

```

C
C PARALLEL SYSTEM - LIKE COMPONENTS - TREATED AS 2-D CASE
C

```

```

DIMENSION PROB(2)
A = PROR(1)*PROB(1)
QTHETA = A + PROB(2)*(1.0-A)
RETURN
END

```

```

7/8/9 ← blank option: standard output

```

PARALLEL SYSTEM - LIKE COMPONENTS - TREATED AS 2-D CASE (EXAMPLE 1)

```

2
20      20
 1      1
 1      0
0.8
0.9
0.95
0.98
0.99
0.999
7/8/9

```

```

← option 1: intermediate printout

```

PARALLEL SYSTEM - LIKE COMPONENTS - TREATED AS 2-D CASE (EXAMPLE 2)

```

2
40      40
 1      1
 1      0
0.8
0.9
0.95
0.98
0.99
0.999
7/8/9

```

```

← option 3: list hypervolumes

```

PARALLEL SYSTEM - LIKE COMPONENTS - TREATED AS 2-D CASE (EXAMPLE 3)

```

2
40      40
 2      2
 1      0
0.8
0.9
0.95
0.98
0.99
0.999
7/8/9
6/7/8/9

```

NOTE: 7/8/9 represents standard CDC 6600 EOF card  
6/7/8/9 represents standard CDC 6600 EOI card

SYSTEM7,T---,CM100000,EC---,MT1. IDENTIFICATION  
 ACCOUNT,S-----,D---,G---,A---,R-,K---.  
 REQUEST,TAPE3,HI. VRN =

REWIND,TAPE3.  
 ATTACH,CONTAP,CONLIM.  
 COPYBF,CONTAP,LGO.  
 FTN,B=LGO1,L,OPT=1.  
 REWIND,LGO1.  
 PREP,LGO1,QTHE.  
 COLLECT,LGO,FTNLIB,QTHE.  
 LGO.  
 UNLOAD,TAPE3.  
 EXIT.  
 UNLOAD,TAPE3.  
 7/8/9

CONLIM is maintained in a permanent file. In this example, a magnetic tape is requested to save the hypervolume structure for subsequent runs. Note that permanent files, rather than tape, can also be used for this purpose. The manual detailing the use of permanent files should be consulted for creating/cataloging a permanent file.

FUNCTION QTHETA(PROB)  
 DIMENSION PROB(5)  
 P1 = (1.0-PROB(1))\*(1.0-PROB(2))  
 P2 = (1.0-PROB(3))\*(1.0-PROB(4))  
 QTHETA = PROB(5) + (1.0-PROB(5))\*(1.0-P1)\*(1.0-P2)  
 RETURN  
 END

7/8/9  
 1

← PARALLEL SYSTEM-FIVE COMPONENTS

Option 4=1; Save hypervolume structure (more than one set can be submitted and more than one structure saved)

5  
 30 20 40 30 20  
 2 1 2 1 1  
 1 1 1 1 0  
 0.8  
 0.9  
 0.95  
 0.98  
 0.99  
 0.999  
 7/8/9  
 6/7/8/9

NOTE: 7/8/9 represents standard CDC 6600 EOF card

6/7/8/9 represents standard CDC 6600 EOI card

SYSTEM10,T---,CM12000,EC---

IDENTIFICATION

ACCOUNT,S-----,D-----,G-----,A-----,R-,K---

ATTACH,OLDPL,CONCLIM,CY=1.  
UPDATE,P=OLDPL,F.  
REWIND,COMPILE.  
FTN,I=COMPILE,L,OPT=1.  
COLLECT,LGO,FTNLIB.  
LGO.

The dimensions of the program CONCLIM must be expanded for this run and two cards of CONCLIM are modified. (Note: increase in core memory required) This information and the function deck are submitted via the UPDATE system of the CDC 6600. UPDATE source of CONCLIM is taken from cycle 1 of the permanent file as shown.

7/8/9  
\*IDENT CHANL  
\*DELETE CONCLIM.116,CONCLIM.117  
DIMENSION NFMAX(9,500),NFMIN(9,500),NFMAXX(9,500),NFMINX(9,500)  
DATA IVSIZE/500/,IVCOL/9/  
\*INSERT CONCLIM.1600  
FUNCTION QTHETA(PROB)

C  
C TWO CHANNEL - TWO OPTION SYSTEM  
C

DIMENSION PROB(9)  
PART1 = (1.0-PROB(1))\*(1.0-PROB(2))\*(1.0-PROB(3))  
P8 = 1.0-PROB(8)  
P7 = 1.0-PROB(7)  
P4 = 1.0-PROB(4)  
P56 = (1.0 - PROB(5)\*PROB(6))  
P456 = P4\*P56  
PART2 = 1.0 - (1.0 - P456)\*(1.0 - P456)  
PART3 = P8\*P7\*PART2  
PART4 = 1.0 - (PROB(4) + P4\*PROB(6))\*\*2  
PART5 = PROB(8)\*P7\*PART4  
PART6 = 1.0 - (PROB(4) + P4\*PROB(5))\*\*2  
PART7 = PROB(7)\*P8\*PART6  
PARTS = PART3 + PART5 + PART7  
THETA = 1.0 - PART1\*PARTS  
QTHETA = PROB(9) + (1.0-PROB(9))\*THETA  
RETURN  
END

\*IDENT identifies this modification to UPDATE

\*DELETE deletes two cards and replaces them with the cards following

\*INSERT places the cards (function deck) immediately following the CONCLIM routine proper

7/8/9



blank option:  
standard output

TWO CHANNEL - TWO OPTION SYSTEM

9								
	54	30	101	32	23	32	43	17
	44							
	1	0	0	1	1	1	1	0
	0							
	0	0	0	1	1	1	1	1
	0							

0.8  
0.90  
0.95  
0.98  
0.99  
0.999  
7/8/9  
6/7/8/9

NOTES: The data cards containing the number of tests, failures, and classification are each continued to second cards.

7/8/9 represents standard CDC 6600 EOF card.

6/7/8/9 represents standard CDC 6600 EOI card.

## APPENDIX E

### EXAMPLES OF OUTPUT RESULTS USING VARIOUS CONLIM OPTIONS

Each of the input data options detailed on the first two pages of the CONLIM listing in Appendix F results in various forms of output and information. This appendix demonstrates the multitude of output forms resulting from these option selections by the user. Should CONLIM prematurely stop as a result of exceeding the designated time limit for the computer run, a brief printout of pertinent information is supplied from CONLIM prior to the run exit.

TIME REQUIRED TO DETERMINE INDEX SET AND HYPERVOLUMES = .001 SECONDS

HYPERVOLUME CROSSCHECK BYPASSED

TIME REQUIRED FOR FIT PROCEDURE = .019 SECONDS

( Standard first page of results which appears at the start of each new set. For multiple  $\alpha$  values only the time for the fit procedure is supplied after the first since the hypervolumes will have been determined previously. )

PARALLEL SYSTEM - LIKE COMPONENTS - TREATED AS 2-D CASE

SYSTEM COMPONENTS  
NUMBER OF TESTS AND FAILURES

1	2
20	20
1	1

ALPHA UPPER CONFIDENCE LIMIT = .8000

SYSTEM FAILURE PROBABILITY Q = .1422641E+00

NUMBER OF HYPERVOLUMES IN INDEX SET = 2  
TOTAL NUMBER OF NTUPLES IN SET = 7

INDIVIDUAL COMPONENT P VALUES ARE AS FOLLOWS

I = 1	P(I) = .7096878E-04
I = 2	P(I) = .1422641E+00

(Standard output of results - for the standard (blank option card) run this will be the only page printed in addition to the timing pages.)

(Option 1 selected - intermediate output)

```
I = 1 PHAT(I) = .4761905E-01
I = 2 PHAT(I) = .4761905E-01
HVALUE STARTING OFF DELTAP = .26153023E+00
I = 1 PHAT(I) = .5284574E-01 QHAT(I) = .9471543E+00
I = 2 PHAT(I) = .5284574E-01 QHAT(I) = .9471543E+00
HVALUE AFTER DELTAP SHIFT = .205653418552E+00
QP VALUE AFTER DELTAP SHIFT = .554908261854E-01
COMPONENT 2 USED TO MAINTAIN CONSTANT Q
DEL VALUE TRIED = .5284574E-02
I = 1 PHAT(I) = .5284574E-01 QHAT(I) = .9471543E+00
I = 2 PHAT(I) = .5284574E-01 QHAT(I) = .9471543E+00
COMPONENT 2 USED TO MAINTAIN CONSTANT Q
DEL VALUE TRIED = .2642287E-02
I = 1 PHAT(I) = .1442557E-02 QHAT(I) = .9985574E+00
I = 2 PHAT(I) = .5548886E-01 QHAT(I) = .9445111E+00
HVALUE STARTING OFF DELTAP = .34107094E+00
I = 1 PHAT(I) = .1813208E-02 QHAT(I) = .9981868E+00
I = 2 PHAT(I) = .6974620E-01 QHAT(I) = .9302538E+00
HVALUE AFTER DELTAP SHIFT = .221418001683E+00
QP VALUE AFTER DELTAP SHIFT = .697492598601E-01
COMPONENT 2 USED TO MAINTAIN CONSTANT Q
DEL VALUE TRIED = .2642287E-02
I = 1 PHAT(I) = .1813208E-02 QHAT(I) = .9981868E+00
I = 2 PHAT(I) = .6974620E-01 QHAT(I) = .9302538E+00
COMPONENT 2 USED TO MAINTAIN CONSTANT Q
DEL VALUE TRIED = .1321143E-02
I = 1 PHAT(I) = .1813208E-02 QHAT(I) = .9981868E+00
I = 2 PHAT(I) = .6974620E-01 QHAT(I) = .9302538E+00
COMPONENT 2 USED TO MAINTAIN CONSTANT Q
DEL VALUE TRIED = .6605717E-03
I = 1 PHAT(I) = .1813208E-02 QHAT(I) = .9981868E+00
I = 2 PHAT(I) = .6974620E-01 QHAT(I) = .9302538E+00
COMPONENT 2 USED TO MAINTAIN CONSTANT Q
DEL VALUE TRIED = .3302858E-03
I = 1 PHAT(I) = .1813208E-02 QHAT(I) = .9981868E+00
I = 2 PHAT(I) = .6974620E-01 QHAT(I) = .9302538E+00
COMPONENT 2 USED TO MAINTAIN CONSTANT Q
DEL VALUE TRIED = .1651429E-03
I = 1 PHAT(I) = .1813208E-02 QHAT(I) = .9981868E+00
I = 2 PHAT(I) = .6974620E-01 QHAT(I) = .9302538E+00
COMPONENT 2 USED TO MAINTAIN CONSTANT Q
DEL VALUE TRIED = .8257146E-04
I = 1 PHAT(I) = .1813208E-02 QHAT(I) = .9981868E+00
I = 2 PHAT(I) = .6974620E-01 QHAT(I) = .9302538E+00
COMPONENT 2 USED TO MAINTAIN CONSTANT Q
DEL VALUE TRIED = .4128573E-04
I = 1 PHAT(I) = .1813208E-02 QHAT(I) = .9981868E+00
I = 2 PHAT(I) = .6974620E-01 QHAT(I) = .9302538E+00
COMPONENT 2 USED TO MAINTAIN CONSTANT Q
DEL VALUE TRIED = .2064287E-04
I = 1 PHAT(I) = .1813208E-02 QHAT(I) = .9981868E+00
I = 2 PHAT(I) = .6974620E-01 QHAT(I) = .9302538E+00
COMPONENT 2 USED TO MAINTAIN CONSTANT Q
DEL VALUE TRIED = .1032143E-04
I = 1 PHAT(I) = .1813208E-02 QHAT(I) = .9981868E+00
I = 2 PHAT(I) = .6974620E-01 QHAT(I) = .9302538E+00
COMPONENT 2 USED TO MAINTAIN CONSTANT Q
DEL VALUE TRIED = .5160716E-05
I = 1 PHAT(I) = .1813208E-02 QHAT(I) = .9981868E+00
I = 2 PHAT(I) = .6974620E-01 QHAT(I) = .9302538E+00
COMPONENT 2 USED TO MAINTAIN CONSTANT Q
```

```

DEL VALUE TRIED = .2580358E-05
I = 1 PHAT(I) = .2068588E-03 QHAT(I) = .9997931E+00
I = 2 PHAT(I) = .6974922E-01 QHAT(I) = .9302508E+00
HVALUE STARTING OFF DELTAP = .22179892E+00
I = 1 PHAT(I) = .2161293E-03 QHAT(I) = .9997839E+00
I = 2 PHAT(I) = .7287508E-01 QHAT(I) = .9271249E+00
HVALUE AFTER DELTAP SHIFT = .200887018676E+00
QP VALUE AFTER DELTAP SHIFT = .728751201759E-01
COMPONENT 2 USED TO MAINTAIN CONSTANT Q
DEL VALUE TRIED = .2580358E-05
I = 1 PHAT(I) = .2161293E-03 QHAT(I) = .9997839E+00
I = 2 PHAT(I) = .7287508E-01 QHAT(I) = .9271249E+00
COMPONENT 2 USED TO MAINTAIN CONSTANT Q
DEL VALUE TRIED = .1290179E-05
I = 1 PHAT(I) = .2161293E-03 QHAT(I) = .9997839E+00
I = 2 PHAT(I) = .7287508E-01 QHAT(I) = .9271249E+00
TIME REQUIRED FOR FIT PROCEDURE = .114 SECONDS

```

( Option 1 printout continued with the time requirement )  
printed after the intermediate output.



(Option 2 selected - determine hypervolumes only)

PARALLEL SYSTEM - LIKE COMPONENTS - TREATED AS 2-D CASE

SYSTEM COMPONENTS  
NUMBER OF TESTS AND FAILURES

1	2
40	40
1	1

ALPHA UPPER CONFIDENCE LIMIT = .8000

HYPERVOLUME ONLY OPTION SELECTED

INDEX SET DETERMINED VIA OPTION 2, ALPHA = .9000 BYPASSED

INDEX SET DETERMINED VIA OPTION 2, ALPHA = .9500 BYPASSED

( The option is indicated and since the fit procedure  
was to be bypassed, so also are any other  $\alpha$  values  
in the set. Hypervolumes need only be calculated  
once for the set. )

(Option 3 selected - list hypervolume structure)

HYPERVOLUME STRUCTURE WITHIN INDEX SET PSI

NUMBER OF HYPERVOLUMES IN INDEX SET = 2  
TOTAL NUMBER OF NTUPLES IN SET = 8

\*\*\*VOLUME 1

J = 1 MIN(J) = 0 MAX(J) = 5  
J = 2 MIN(J) = 0 MAX(J) = 0

\*\*\*VOLUME 2

J = 1 MIN(J) = 0 MAX(J) = 1  
J = 2 MIN(J) = 1 MAX(J) = 1

( The structure is listed prior to any other action -  
standard output and/or intermediate output would  
follow. )

(Options 2 and 3 selected - determine hypervolumes and list)

PARALLEL SYSTEM - LIKE COMPONENTS - TREATED AS 2-D CASE

SYSTEM COMPONENTS  
NUMBER OF TESTS AND FAILURES

1	2
40	40
1	1

ALPHA UPPER CONFIDENCE LIMIT = .8000

HYPERVOLUME ONLY OPTION SELECTED

INDEX SET COMPOSITION PREVIOUSLY LISTED VIA OPTION 3, ALPHA = .9000 BYPASSED

INDEX SET COMPOSITION PREVIOUSLY LISTED VIA OPTION 3, ALPHA = .9500 BYPASSED

(All hypervolumes would be printed as shown on the previous page.  
However, processing of the set will stop without performing any  
further calculations. Multiple  $\alpha$  values in the set are bypassed.)

(Option 4 = 1 selected - save index set for subsequent runs)

TIME REQUIRED TO DETERMINE INDEX SET AND HYPERVOLUMES = .001 SECONDS

HYPERVOLUME STRUCTURE SAVED ON FILE 1 OF TAPE3

HYPERVOLUME CROSSCHECK BYPASSED

TIME REQUIRED FOR FIT PROCEDURE = .020 SECONDS

( This information is supplied along with any other options selected. If only option 4 is selected CONLIM will complete the fit procedure and supply a standard report. Other options selected will produce additional output as described in this appendix. )

(Option 4 = 2 selected - read hypervolumes from tape)

INDEX SET AND HYPERVOLUMES INPUT FROM TAPE4

HYPERVOLUME CROSSCHECK BYPASSED

TIME REQUIRED FOR FIT PROCEDURE = .119 SECONDS

( This message is supplied if the system described on tape  
matches the system described via the data set. Notice  
that no time is given for construction of the index set  
since it is taken from tape. )

(Option 4 = 2 Continued)

PARALLEL SYSTEM - LIKE COMPONENTS - TREATED AS 2-D CASE

SYSTEM COMPONENTS  
NUMBER OF TESTS AND FAILURES

1	2
40	40
3	3

ALPHA UPPER CONFIDENCE LIMIT = .8000

SYSTEM FAILURE PROBABILITY Q = .1337244E+00

NUMBER OF HYPERVOLUMES IN INDEX SET = 4  
TOTAL NUMBER OF NTUPLES IN SET = 32

INDIVIDUAL COMPONENT P VALUES ARE AS FOLLOWS

I = 1	P(I) = .2020070E-01
I = 2	P(I) = .1333707E+00

(This report can be compared to the situation when  
the systems did not agree.)

(Option 4 = 2 selected - read hypervolume structure from tape)

PARALLEL SYSTEM - LIKE COMPONENTS - TREATED AS 2-D CASE

SYSTEM COMPONENTS  
NUMBER OF TESTS AND FAILURES

1	2
20	20
1	1

DATA DESCRIBED AS INPUT TO CONLIM DID NOT MATCH  
REQUESTED DATA FROM TAPE4 - SET BYPASSED

INFORMATION FROM TAPE4 LISTED BELOW

I = 1	N(I) = 40	NX(I) = 3	NTYPE(I) = 1
I = 2	N(I) = 40	NX(I) = 3	NTYPE(I) = 0

( In this situation, the information supplied via the data set did not agree with that on tape and thus would not have produced the proper hypervolume structure. A diagnostic message is supplied, multiple  $\alpha$  values in the set bypassed, and the next set is processed. )

(Option 5 selected - check the hypervolumes criteria)

COMPARISON CHECKS ON Q VALUES FOR MINMAX LIMITS

Q VALUE USED FOR INDEX SET CRITERIA, QLIM = .761661807580E-01

KVOL	QMIN	QLIM-QMIN	QMAX	QLIM-QMAX
1	.243629197711E-01	.518E-01	.686345966958E-01	.753E-02
2	.481589461181E-01	.280E-01	.740740740741E-01	.209E-02
3	.719549724652E-01	.421E-02	.761661807580E-01	0.

HYPERVOLUME CHECK INDICATES GOOD SET

( To be included in the index set all n-tuples must satisfy the set criteria, and hence the upper and lower bounds of hypervolumes must also meet that criteria. This crosscheck indicates if this condition exists. Note that we must always have

$QLIM - QMIN \geq 0$   
 $QLIM - QMAX \geq 0$



(Option 5 selected - continued)

TIME REQUIRED TO DETERMINE INDEX SET AND HYPERVOLUMES = .002 SECONDS

TIME REQUIRED TO PERFORM HYPERVOLUME CROSSCHECK = .014 SECONDS

TIME REQUIRED FOR FIT PROCEDURE = .045 SECONDS

(Timing for the crosscheck is also supplied  
when this option is selected.)

(Option 6 = 0 selected - do not take branches if encountered)

SERIES SYSTEM GIVING BRANCHES FOR OPTION 6

SYSTEM COMPONENTS  
NUMBER OF TESTS AND FAILURES

1	2	3
20	15	10
1	0	0

ALPHA UPPER CONFIDENCE LIMIT = .6000

NUMBER OF HYPERVOLUMES IN INDEX SET = 1  
TOTAL NUMBER OF NTUPLES IN SET = 2

```
*****  
*  
* OSCILLATION BETWEEN COMPONENT P VALUES *  
* ENCOUNTERED - EXECUTION FOR THIS ALPHA VALUE *  
* IS TERMINATED *  
* BELOW ARE LISTED THE INDIVIDUAL P VALUES UPON *  
* TERMINATION WITH OSCILLATING COMPONENTS MARKED *  
* I = 1 P(I) = .5158699E-01 *** *  
* I = 2 P(I) = .1522537E-03 *  
* I = 3 P(I) = .5737241E-01 *** *  
*  
*****
```

( Should the situation arise when two or more components oscillate without advancing significantly toward a maximum and option 6 is not set, a message is supplied to the user. Further processing on this  $\alpha$  is halted. CONLIM will proceed to perform calculations for additional  $\alpha$  values and sets. )

(Option 6 = 1 selected - take individual branches upon oscillation)

SERIES SYSTEM GIVING BRANCHES FOR OPTION 6

SYSTEM COMPONENTS  
NUMBER OF TESTS AND FAILURES

1	2	3
20	15	10
1	0	0

ALPHA UPPER CONFIDENCE LIMIT = .6000

SYSTEM FAILURE PROBABILITY Q = .1089992E+00

NUMBER OF HYPERVOLUMES IN INDEX SET = 1

TOTAL NUMBER OF NTUPLES IN SET = 2

INDIVIDUAL COMPONENT P VALUES ARE AS FOLLOWS

I = 1	P(I) = .4735771E-01
I = 2	P(I) = .1189675E-05
I = 3	P(I) = .6164032E-01

RESULTS SHOWN ABOVE WERE OBTAINED BY HOLDING  
COMPONENT 1 FIXED AS THE SLACK COMPONENT VIA OPTION 6

( If option 6 is selected and oscillation occurs, CONLIM will hold each of the oscillating components fixed and proceed to finish the calculations. We previously noted that components 1 and 3 were oscillating. The next page shows 3 being held fixed. )

(Option 6 = 1 continued)

SERIES SYSTEM GIVING BRANCHES FOR OPTION 6

SYSTEM COMPONENTS  
NUMBER OF TESTS AND FAILURES

1	2	3
20	15	10
1	0	0

ALPHA UPPER CONFIDENCE LIMIT = .6000

SYSTEM FAILURE PROBABILITY Q = .1089217E+00

NUMBER OF HYPERVOLUMES IN INDEX SET = 1  
TOTAL NUMBER OF NTUPLES IN SET = 2

INDIVIDUAL COMPONENT P VALUES ARE AS FOLLOWS

I = 1	P(I) = .5984061E-01
I = 2	P(I) = .8799240E-06
I = 3	P(I) = .4908024E-01

RESULTS SHOWN ABOVE WERE OBTAINED BY HOLDING  
COMPONENT 3 FIXED AS THE SLACK COMPONENT VIA OPTION 6

( As on the preceding page, component 3 is now fixed.  
CONLIM saves all information at the point of the branch  
and proceeds from there without retracing the early  
portion of the path. )

END OF ANALYSIS - PARALLEL SYSTEM - LIKE COMPONENTS - TREATED AS 2-D CASE

(Standard last page of a data set. The title  
used for the set is repeated at the end of the  
set analysis.)

APPENDIX F  
LISTING OF CONLIM

C	PROGRAM CONLIM(INPUT,OUTPUT,TAPE3,TAPE4,TAPE5=INPUT)	CONLIM	2
C		CONLIM	3
C	THIS ROUTINE PERFORMS THE CALCULATIONS NECESSARY TO ESTABLISH AN	CONLIM	4
C	UPPER CONFIDENCE LIMIT FOR SYSTEM FAILURE PROBABILITY.	CONLIM	5
C		CONLIM	6
C	* * * * *	CONLIM	7
C	ISSUED BY SANDIA LABORATORIES,	CONLIM	8
C	A PRIME CONTRACTOR TO THE	CONLIM	9
C	UNITED STATES ATOMIC ENERGY COMMISSION	CONLIM	10
C	* * * * * NOTICE * * * * *	CONLIM	11
C	* THIS REPORT WAS PREPARED AS AN ACCOUNT OF WORK SPONSORED BY THE	CONLIM	12
C	UNITED STATES GOVERNMENT. NEITHER THE UNITED STATES NOR THE	CONLIM	13
C	UNITED STATES ATOMIC ENERGY COMMISSION, NOR ANY OF THEIR	CONLIM	14
C	EMPLOYEES, NOR ANY OF THEIR CONTRACTORS, SUBCONTRACTORS, OR THEIR	CONLIM	15
C	EMPLOYEES, MAKES ANY WARRANTY, EXPRESS OR IMPLIED, OR ASSUMES ANY	CONLIM	16
C	LEGAL LIABILITY OR RESPONSIBILITY FOR THE ACCURACY, COMPLETENESS	CONLIM	17
C	OR USEFULNESS OF ANY INFORMATION, APPARATUS, PRODUCT OR PROCESS	CONLIM	18
C	DISCLOSED, OR REPRESENTS THAT ITS USE WOULD NOT INFRINGE	CONLIM	19
C	PRIVATELY OWNED RIGHTS.	CONLIM	20
C	* * * * *	CONLIM	21
C	* THE BASIC REFERENCE DOCUMENT FOR THIS CODE IS SLA-73-0563,	CONLIM	22
C	SEPTEMBER 1973.	CONLIM	23
C	* * * * *	CONLIM	24
C	* THIS CODE HAS BEEN APPROVED FOR PUBLIC RELEASE WITHIN THE	CONLIM	25
C	UNITED STATES. NO FOREIGN DISSEMINATION IS PERMITTED WITHOUT	CONLIM	26
C	SPECIFIC APPROVAL FROM THE U.S. ATOMIC ENERGY COMMISSION.	CONLIM	27
C	* * * * *	CONLIM	28
C	WRITTEN BY RONALD D. HALBGEWACHS	CONLIM	29
C	SYSTEMS SOFTWARE DIVISION 2641	CONLIM	30
C	SANDIA LABORATORIES	CONLIM	31
C		CONLIM	32
C		CONLIM	33
C	RELEASE DATE MAY,1973.	CONLIM	34
C		CONLIM	35
C	* * * * *	CONLIM	36
C		CONLIM	37
C	INPUT DATA FORMAT	CONLIM	38
C		CONLIM	39
C	CARD 1 - OPTION INDICATORS	CONLIM	40
C		CONLIM	41
C	BLANK CARD INDICATES NORMAL EXECUTION WITH STANDARD	CONLIM	42
C	OUTPUT RETURNED TO THE USER	CONLIM	43
C		CONLIM	44
C	NON-BLANK CARD INDICATES SPECIAL OPTIONS TO BE TAKEN	CONLIM	45
C	AND SPECIAL OUTPUT IN ADDITION TO STANDARD OUTPUT	CONLIM	46
C		CONLIM	47
C	COL. 1 = 1, PRINT INTERMEDIATE STEP VALUES OF	CONLIM	48
C	P TERMS, H VALUES, AND F VALUES FOR	CONLIM	49
C	EACH STEP IN THE FIT PROCESS	CONLIM	50
C		CONLIM	51
C	COL. 2 = 1, DETERMINE HYPERVOLUMES ONLY, DO NOT	CONLIM	52
C	CALCULATE FAILURE PROBABILITY.	CONLIM	53
C		CONLIM	54
C	COL. 3 = 1, LIST COMPLETE SET OF HYPERVOLUMES	CONLIM	55

C		CONCLIM	56
C		CONCLIM	57
C	COL. 4 = 1, SAVE HYPERVOLUME STRUCTURE ON TAPE3	CONCLIM	58
C	FOR LATER RUNS - IF MORE THAN ONE	CONCLIM	59
C	INDEX SET TO BE SAVED (SEVERAL PROBLEMS	CONCLIM	60
C	IN THE DATA SET) SEPARATE FILES WILL	CONCLIM	61
C	BE SAVED	CONCLIM	62
C	= 2, HYPERVOLUMES PREVIOUSLY SAVED ON	CONCLIM	63
C	MAGNETIC TAPE - READ FROM TAPE4	CONCLIM	64
C	(TAPE4 MUST BE POSITIONED PRIOR TO	CONCLIM	65
C	EXECUTION)	CONCLIM	66
C	COL. 5 = 1, PERFORM CROSSCHECK ON HYPERVOLUMES	CONCLIM	67
C	FOR MATCHING INDEX SET CRITERIA	CONCLIM	68
C		CONCLIM	69
C	COL. 6 = 1, IF COMPONENT OSCILLATION OCCURS,	CONCLIM	70
C	TAKE EACH OF THE SEPARATE BRANCHES	CONCLIM	71
C	BEFORE CONTINUING	CONCLIM	72
C		CONCLIM	73
C	CARD 2 - TITLE OF SYSTEM UNDER STUDY (8A10)	CONCLIM	74
C		CONCLIM	75
C	CARD 3 - NUMBER OF INDIVIDUAL COMPONENTS IN SYSTEM (I3)	CONCLIM	76
C		CONCLIM	77
C	CARD 4 - NUMBER OF TESTS PERFORMED ON EACH COMPONENT (8I10)	CONCLIM	78
C	(NOTE - DATA CAN BE CONTINUED TO AS MANY CARDS	CONCLIM	79
C	AS NECESSARY)	CONCLIM	80
C		CONCLIM	81
C	CARD 5 - NUMBER OF FAILURES ON EACH COMPONENT DURING	CONCLIM	82
C	TESTING (8I10)	CONCLIM	83
C	(NOTE - DATA CAN BE CONTINUED TO AS MANY CARDS	CONCLIM	84
C	AS NECESSARY CONFORMING WITH PREVIOUS CARDS)	CONCLIM	85
C		CONCLIM	86
C	CARD 6 - INDICATORS OF COMPONENT IN PARALLEL OR	CONCLIM	87
C	SERIES (8I10) (NOTE - CONTINUE DATA AS PER	CONCLIM	88
C	THE PRECEDING COMPONENT DATA)	CONCLIM	89
C		CONCLIM	90
C	0 -- INDICATES SERIES LINKAGE	CONCLIM	91
C	1 -- INDICATES PARALLEL LINKAGE	CONCLIM	92
C		CONCLIM	93
C	CARD 7 - ALPHA UPPER CONFIDENCE CRITERIA (F10.5)	CONCLIM	94
C	(NOTE - AS MANY ALPHA VALUES AS DESIRED CAN BE	CONCLIM	95
C	SUPPLIED, ONE PER CARD)	CONCLIM	96
C		CONCLIM	97
C	CARD 8 - END OF FILE CARD (7-8-9 IN FIRST COLUMN)	CONCLIM	98
C		CONCLIM	99
C	AS MANY SETS OF DATA AS DESIRED CAN BE INPUT PROVIDED EACH	CONCLIM	100
C	SET (CARD 1 - CARD 7 INCLUSIVE) IS SEPARATED BY CARD 8 AND	CONCLIM	101
C	THE FINAL SET ALSO CONTAINS CARD 8.	CONCLIM	102
C		CONCLIM	103
C	INTEGER OPT	CONCLIM	104
C	EXTERNAL SUB	CONCLIM	105
C	DIMENSION N(50),NX(50),FN(50),FNX(50),PHAT(50),QHAT(50),	CONCLIM	106
C	1FACT(50),M(50),MX(50),MTYPE(50),NTYPE(50),NSTAR(50),OPT.(6),	CONCLIM	107
C	2TITLE(8),ID(10),VAL(11),SAVAL(10),IDINV(10)	CONCLIM	108
C	COMMON /QVAR/N,FN,FNX,PHAT,QHAT,IFLAG,IVOL,IVSIZE,QLIM,IVCOL,OPT,	CONCLIM	109



1	ITOTAL,NSTAR	CONLIM	110
	COMMON /PSIFLG/IPSIFG	CONLIM	111
	COMMON /FACTR/ FACT	CONLIM	112
	COMMON /TYPE/NTYPE	CONLIM	113
	COMMON /FIRST/ IFIRST,DEL,IFREEZ,NIDS,ID,NLAST,IVAL,VAL,	CONLIM	114
1	SAVAL,IDINV	CONLIM	115
	EQUIVALENCE (PHAT(1),M(1)),(GHAT(1),MX(1)),(NSTAR(1),MTYPE(1))	CONLIM	116
	DIMENSION NFMAX(8,500),NFMIN(8,500),NFMAXX(8,500),NFMINX(8,500)	CONLIM	117
	DATA IVSIZE/500/,IVCOL/8/	CONLIM	118
C		CONLIM	119
C	RECOVERY FLAG SET FOR ABNORMAL TERMINATION	CONLIM	120
C		CONLIM	121
	CALL RECOVR(SUB,63,0)	CONLIM	122
C		CONLIM	123
C	BUILD SMALL FACTORIAL ARRAY TO AVOID SOME UNNECESSARY CALCULATION	CONLIM	124
C		CONLIM	125
	FACT(1) = 1.0	CONLIM	126
	DO 20 I=1,49	CONLIM	127
	XI = I + 1	CONLIM	128
	FACT(I+1) = XI*FACT(I)	CONLIM	129
20	CONTINUE	CONLIM	130
	IVS = IVSIZE	CONLIM	131
	IVCOLS = IVCOL	CONLIM	132
	IFILE = 0	CONLIM	133
	IFREEZ = 0	CONLIM	134
C		CONLIM	135
C	READ INPUT DATA	CONLIM	136
C		CONLIM	137
	READ 30, OPT	CONLIM	138
30	FORMAT (6I1)	CONLIM	139
35	IALP = 1	CONLIM	140
	IFLAG = 0	CONLIM	141
	NINBAD = 0	CONLIM	142
	READ 40, TITLE	CONLIM	143
40	FORMAT (8A10)	CONLIM	144
	READ 60, NCOM	CONLIM	145
60	FORMAT (I3)	CONLIM	146
	READ 80, (N(I),I=1,NCOM)	CONLIM	147
80	FORMAT (8I10)	CONLIM	148
	READ 80, (NX(I),I=1,NCOM)	CONLIM	149
	READ 80, (NTYPE(I),I=1,NCOM)	CONLIM	150
	DO 100 I=1,NCOM	CONLIM	151
	FN(I) = N(I)	CONLIM	152
	FNX(I) = NX(I)	CONLIM	153
100	CONTINUE	CONLIM	154
110	READ (5,120) ALPHA	CONLIM	155
120	FORMAT (F10.5)	CONLIM	156
	IF (EOF(5)) 300,121	CONLIM	157
121	IF (IALP.GT.1) GO TO 1470	CONLIM	158
	IF (OPT(4).LE.1) GO TO 131	CONLIM	159
	READ (4,80) MCOM	CONLIM	160
	READ (4,80) (M(I),I=1,MCOM),(MX(I),I=1,MCOM),(MTYPE(I),I=1,MCOM)	CONLIM	161
	IF (MCOM.NE.NCOM) GO TO 123	CONLIM	162
	DO 122 I=1,NCOM	CONLIM	163

IF (N(I).NE.M(I)) GO TO 123	CONCLIM	164
IF (NX(I).NE.MX(I)) GO TO 123	CONCLIM	165
IF (NTYPE(I).NE.MTYPE(I)) GO TO 123	CONCLIM	166
122 CONTINUE	CONCLIM	167
GO TO 125	CONCLIM	168
123 NINBAD = 1	CONCLIM	169
GO TO 150	CONCLIM	170
125 NVOL = 0	CONCLIM	171
ITOTAL = 0	CONCLIM	172
IECS = 1	CONCLIM	173
NWORDS = IVSIZE*IVCOL	CONCLIM	174
THYP = 0.0	CONCLIM	175
126 IN = 1	CONCLIM	176
127 READ (4,128) (NFMIN(IJ,IN),NFMAX(IJ,IN),IJ=1,NCOM)	CONCLIM	177
128 FORMAT (2I4)	CONCLIM	178
IF (EOF(4)) 130,129	CONCLIM	179
129 ITUP = 1	CONCLIM	180
DO 1290 IT=1,NCOM	CONCLIM	181
ITUP = ITUP*(NFMAX(IT,IN) - NFMIN(IT,IN) + 1)	CONCLIM	182
1290 CONTINUE	CONCLIM	183
ITOTAL = ITOTAL + ITUP	CONCLIM	184
IN = IN + 1	CONCLIM	185
NVOL = NVOL + 1	CONCLIM	186
IF (IN.LE.IVSIZE) GO TO 127	CONCLIM	187
CALL WRITEC(NFMIN,IECS,NWORDS)	CONCLIM	188
IECS = IECS + NWORDS	CONCLIM	189
CALL WRITEC(NFMAX,IECS,NWORDS)	CONCLIM	190
IECS = IECS + NWORDS	CONCLIM	191
IFLAG = IFLAG + 1	CONCLIM	192
GO TO 126	CONCLIM	193
130 IVOL = IN - 1	CONCLIM	194
IF (IVOL.EQ.0) GO TO 137	CONCLIM	195
NWORDS = IVOL*IVCOL	CONCLIM	196
CALL WRITEC(NFMIN,IECS,NWORDS)	CONCLIM	197
IECS = IECS + NWORDS	CONCLIM	198
CALL WRITEC(NFMAX,IECS,NWORDS)	CONCLIM	199
IF (OPT(3).EQ.1) CALL PSI(NCOM,NVOL,NFMIN,NFMAX,NFMINX,NFMAXX,	CONCLIM	200
1 IVS,IVCOLS,IER)	CONCLIM	201
GO TO 137	CONCLIM	202
C	CONCLIM	203
C DETERMINE THE INDEX SET AND INITIAL H FUNCTION VALUE FOR THE	CONCLIM	204
C BEGINNING PHAT PROBABILITIES - START THE BALL ROLLING.	CONCLIM	205
C	CONCLIM	206
131 CALL SECOND(THYP1)	CONCLIM	207
CALL PSI(NCOM,NVOL,NFMIN,NFMAX,NFMINX,NFMAXX,IVS,IVCOLS,IER)	CONCLIM	208
CALL SECOND(THYP2)	CONCLIM	209
THYP = THYP2 - THYP1	CONCLIM	210
IF (OPT(4).NE.1) GO TO 137	CONCLIM	211
WRITE (3,80) NCOM	CONCLIM	212
WRITE (3,80) (N(I),I=1,NCOM),(NX(I),I=1,NCOM),(NTYPE(I),I=1,NCOM)	CONCLIM	213
MFLAG = 0	CONCLIM	214
IECS = 1	CONCLIM	215
NWORDS = IVSIZE*IVCOL	CONCLIM	216
IFLG = 0	CONCLIM	217

132	IF (IFLAG.EQ.MFLAG) GO TO 135	CONCLIM	218
	IVEND = IVSIZE	CONCLIM	219
133	CALL READEC(NFMIN,IECS,NWORDS)	CONCLIM	220
	IECS = IECS + NWORDS	CONCLIM	221
	CALL READEC(NFMAX,IECS,NWORDS)	CONCLIM	222
	IECS = IECS + NWORDS	CONCLIM	223
1330	DO 134 IK=1,IVEND	CONCLIM	224
	WRITE (3,128) (NFMIN(IJ,IK),NFMAX(IJ,IK), IJ=1,NCOM)	CONCLIM	225
134	CONTINUE	CONCLIM	226
	MFLAG = MFLAG + 1	CONCLIM	227
	IF (IFLG.EQ.1) GO TO 136	CONCLIM	228
	GO TO 132	CONCLIM	229
135	IF (IVOL.EQ.0) GO TO 136	CONCLIM	230
	IVEND = IVOL	CONCLIM	231
	NWORDS = IVOL*IVCOL	CONCLIM	232
	IFLG = 1	CONCLIM	233
	IF (IFLAG.EQ.0) GO TO 1330	CONCLIM	234
	GO TO 133	CONCLIM	235
136	ENDFILE 3	CONCLIM	236
	IFILE = IFILE + 1	CONCLIM	237
137	TCOMP = 0.0	CONCLIM	238
	IF (OPT(5).EQ.0) GO TO 138	CONCLIM	239
	CALL SECOND(TCOMP1)	CONCLIM	240
	CALL COMPAQ(NCOM,NFMIN,NFMAX,IVS,IVCOLS)	CONCLIM	241
	CALL SECOND(TCOMP2)	CONCLIM	242
	TCOMP = TCOMP2 - TCOMP1	CONCLIM	243
138	PRINT 139	CONCLIM	244
139	FORMAT (1H1///)	CONCLIM	245
	IF (OPT(4).EQ.2) GO TO 141	CONCLIM	246
	PRINT 140, THYP	CONCLIM	247
140	FORMAT (20X,56HTIME REQUIRED TO DETERMINE INDEX SET AND HYPERVOLUM	CONCLIM	248
	IES = ,F9.3, 8H SECONDS/)	CONCLIM	249
	IF (OPT(4).NE.1) GO TO 143	CONCLIM	250
	PRINT 1400, IFILE,NVOL	CONCLIM	251
1400	FORMAT (/20X,35HHYPERVOLUME STRUCTURE SAVED ON FILE,I2,14H OF TAPE	CONCLIM	252
	13 (,16,15H HYPERVOLUMES )/)	CONCLIM	253
	GO TO 143	CONCLIM	254
141	PRINT 142	CONCLIM	255
142	FORMAT (20X,43HINDEX SET AND HYPERVOLUMES INPUT FROM TAPE4/)	CONCLIM	256
143	IF (OPT(5).EQ.0) GO TO 145	CONCLIM	257
	PRINT 144, TCOMP	CONCLIM	258
144	FORMAT (20X,50HTIME REQUIRED TO PERFORM HYPERVOLUME CROSSCHECK = ,	CONCLIM	259
	1F9.3,8H SECONDS/)	CONCLIM	260
	GO TO 147	CONCLIM	261
145	PRINT 146	CONCLIM	262
146	FORMAT (20X,31HHYPERVOLUME CROSSCHECK BYPASSED/)	CONCLIM	263
147	IF (OPT(2).EQ.1) GO TO 150	CONCLIM	264
1470	DO 148 I=1,NCOM	CONCLIM	265
	PHAT(I) = (FN(I)+1.0)/(FN(I)+2.0)	CONCLIM	266
148	CONTINUE	CONCLIM	267
	CALL SECOND(TFIT1)	CONCLIM	268
	CALL FIT(NCOM,ALPHA,GOFP,NFMIN,NFMAX,IVS,IVCOLS,IERR)	CONCLIM	269
	IF (IERR.EQ.3) GO TO 150	CONCLIM	270
	CALL SECOND(TFIT2)	CONCLIM	271

TFIT = TFIT2 - TFIT1	CONCLIM	272
PRINT 149, TFIT	CONCLIM	273
149 FORMAT (20X,34H TIME REQUIRED FOR FIT PROCEDURE = ,F9.3,8H SECONDS)	CONCLIM	274
150 PRINT 151, TITLE	CONCLIM	275
151 FORMAT (1H1///27X,8A10//)	CONCLIM	276
PRINT 152	CONCLIM	277
152 FORMAT (58X,17H SYSTEM COMPONENTS/53X,28H NUMBER OF TESTS AND FAILUR	CONCLIM	278
IES/)	CONCLIM	279
ILIST = NCOM.	CONCLIM	280
ISTRT = 1	CONCLIM	281
IEND = 0	CONCLIM	282
153 IF (ILIST.LE.20) GO TO 156	CONCLIM	283
IEND = IEND + 20	CONCLIM	284
PRINT 154, (I,I=ISTRT,IEND)	CONCLIM	285
154 FORMAT (27X,20I4)	CONCLIM	286
PRINT 154, (N(I),I=ISTRT,IEND)	CONCLIM	287
PRINT 154, (NX(I),I=ISTRT,IEND)	CONCLIM	288
PRINT 155	CONCLIM	289
155 FORMAT (///)	CONCLIM	290
ILIST = ILIST - 20	CONCLIM	291
ISTRT = ISTRT + 20	CONCLIM	292
GO TO 153	CONCLIM	293
156 IF (ILIST.LT.16) GO TO 158	CONCLIM	294
PRINT 157, (I,I=ISTRT,NCOM)	CONCLIM	295
157 FORMAT (34X,20I4)	CONCLIM	296
PRINT 157, (N(I),I=ISTRT,NCOM)	CONCLIM	297
PRINT 157, (NX(I),I=ISTRT,NCOM)	CONCLIM	298
GO TO 170	CONCLIM	299
158 IF (ILIST.LT.12) GO TO 160	CONCLIM	300
PRINT 159, (I,I=ISTRT,NCOM)	CONCLIM	301
159 FORMAT (42X,16I4)	CONCLIM	302
PRINT 159, (N(I),I=ISTRT,NCOM)	CONCLIM	303
PRINT 159, (NX(I),I=ISTRT,NCOM)	CONCLIM	304
GO TO 170	CONCLIM	305
160 IF (ILIST.LT.8) GO TO 162	CONCLIM	306
PRINT 161, (I,I=ISTRT,NCOM)	CONCLIM	307
161 FORMAT (48X,12I4)	CONCLIM	308
PRINT 161, (N(I),I=ISTRT,NCOM)	CONCLIM	309
PRINT 161, (NX(I),I=ISTRT,NCOM)	CONCLIM	310
GO TO 170	CONCLIM	311
162 IF (ILIST.LT.4) GO TO 164	CONCLIM	312
PRINT 163, (I,I=ISTRT,NCOM)	CONCLIM	313
163 FORMAT (56X,8I4)	CONCLIM	314
PRINT 163, (N(I),I=ISTRT,NCOM)	CONCLIM	315
PRINT 163, (NX(I),I=ISTRT,NCOM)	CONCLIM	316
GO TO 170	CONCLIM	317
164 PRINT 165, (I,I=ISTRT,NCOM)	CONCLIM	318
165 FORMAT (63X,4I4)	CONCLIM	319
PRINT 165, (N(I),I=ISTRT,NCOM)	CONCLIM	320
PRINT 165, (NX(I),I=ISTRT,NCOM)	CONCLIM	321
170 IF (NINBAD.EQ.0) GO TO 171	CONCLIM	322
PRINT 1700	CONCLIM	323
1700 FORMAT (///40X,47H DATA DESCRIBED AS INPUT TO CONCLIM DID NOT MATCH/	CONCLIM	324
140X,40H REQUESTED DATA FROM TAPE4 - SET BYPASSED//40X,35H INFORMATIO	CONCLIM	325

2N FROM TAPE4 LISTED BELOW//)	CONCLIM	326
PRINT 1710, (I,M(I),MX(I),MTYPE(I),I=1,MCOM)	CONCLIM	327
1710 FORMAT (35X,4HI = ,I2,5X,7HN(I) = ,I4,5X,8HNX(I) = ,I4,5X,	CONCLIM	328
111HNTYPE(I) = ,I1)	CONCLIM	329
GO TO 1730	CONCLIM	330
171 IF (OPT(2).EQ.0) GO TO 174	CONCLIM	331
PRINT 175, ALPHA	CONCLIM	332
PRINT 172	CONCLIM	333
172 FORMAT (///20X,324HYPERVOLUME ONLY OPTION SELECTED//)	CONCLIM	334
1730 READ (5,120) ALPHA	CONCLIM	335
IF (EOF(5)) 300,1732	CONCLIM	336
1732 IF (NINBAD.EQ.1) GO TO 1730	CONCLIM	337
IF (OPT(3).NE.1) GO TO 1736	CONCLIM	338
PRINT 1734, ALPHA	CONCLIM	339
1734 FORMAT (/20X,62HINDEX SET COMPOSITION PREVIOUSLY LISTED VIA OPTION	CONCLIM	340
1 3, ALPHA = ,F9.4,9H BYPASSED//)	CONCLIM	341
GO TO 1730	CONCLIM	342
1736 PRINT 1738, ALPHA	CONCLIM	343
1738 FORMAT (/20X,43HINDEX SET DETERMINED VIA OPTION 2, ALPHA = ,F9.4,	CONCLIM	344
19H BYPASSED//)	CONCLIM	345
GO TO 1730	CONCLIM	346
174 PRINT 175, ALPHA	CONCLIM	347
175 FORMAT (///43X,31HALPHA UPPER CONFIDENCE LIMIT = ,F9.4)	CONCLIM	348
IF (IFKEEZ .GT. 0) GO TO 200	CONCLIM	349
PRINT 178, QOFP	CONCLIM	350
178 FORMAT (///43X,30HSYSTEM FAILURE PROBABILITY Q = ,E14.7)	CONCLIM	351
PRINT 180, NVOL,ITOTAL	CONCLIM	352
180 FORMAT (///43X,38HNUMBER OF HYPERVOLUMES IN INDEX SET = ,I5/	CONCLIM	353
143X,33HTOTAL NUMBER OF NTUPLES IN SET = ,I6)	CONCLIM	354
PRINT 182	CONCLIM	355
182 FORMAT (///43X,45HINDIVIDUAL COMPONENT P VALUES ARE AS FOLLOWS //)	CONCLIM	356
PRINT 184, (I,PHAT(I), I=1,NCOM)	CONCLIM	357
184 FORMAT (50X,4HI = ,I2,5X,6HP(I) = ,E14.7)	CONCLIM	358
IALP = 2	CONCLIM	359
IF (IERR.NE.2) GO TO 195	CONCLIM	360
PRINT 190	CONCLIM	361
190 FORMAT (///40X,	CONCLIM	362
1 51H*****//40X,	CONCLIM	363
2 51H* */40X,	CONCLIM	364
3 51H* NEAR-ZERO SERIES COMPONENTS MAY INDICATE THAT */40X,	CONCLIM	365
4 51H* CONCLIM RESULTS HAVE NOT REFLECTED TRUE SYSTEM */40X,	CONCLIM	366
5 51H* VALUES */40X,	CONCLIM	367
6 51H* */40X,	CONCLIM	368
7 51H*****//40X,)	CONCLIM	369
195 PRINT 139	CONCLIM	370
GO TO 110	CONCLIM	371
C	CONCLIM	372
C OSCILLATION BETWEEN COMPONENTS WITHOUT CONVERGENCE	CONCLIM	373
C	CONCLIM	374
200 IF (OPT(6).EQ.1)GO TO 240	CONCLIM	375
PRINT 180, NVOL,ITOTAL	CONCLIM	376
PRINT 205	CONCLIM	377
205 FORMAT (///40X,	CONCLIM	378
1 51H*****//40X,	CONCLIM	379

2	51H*		*/40X,	CONLIM	380
3	51H*	OSCILLATION BETWEEN COMPONENT P VALUES	*/40X,	CONLIM	381
4	51H*	ENCOUNTERED - EXECUTION FOR THIS ALPHA VALUE	*/40X,	CONLIM	382
5	51H*	IS TERMINATED	*/40X,	CONLIM	383
6	51H*	BELOW ARE LISTED THE INDIVIDUAL P VALUES UPON	*/40X,	CONLIM	384
7	51H*	TERMINATION WITH OSCILLATING COMPONENTS MARKED *)		CONLIM	385
		DO 230 I=1,NCOM		CONLIM	386
		DO 210 J=1,NIDS		CONLIM	387
		IF (I.EQ.ID(J)) GO TO 220		CONLIM	388
210		CONTINUE		CONLIM	389
		PRINT 215, I,PHAT(I)		CONLIM	390
215		FORMAT (40X,14H* I = ,I2,5X,6HP(I) = ,E14.7,10H	*)	CONLIM	391
		GO TO 230		CONLIM	392
220		PRINT 225, I,PHAT(I)		CONLIM	393
225		FORMAT (40X,14H* I = ,I2,5X,6HP(I) = ,E14.7,10H ***	*)	CONLIM	394
230		CONTINUE		CONLIM	395
		PRINT 235		CONLIM	396
235		FORMAT (40X,		CONLIM	397
	1	51H*	*/40X,	CONLIM	398
	2	51H*****		CONLIM	399
		IFREEZ = 0		CONLIM	400
		GO TO 195		CONLIM	401
C				CONLIM	402
C		TAKE BRANCHES FOR USER INFORMATION		CONLIM	403
C				CONLIM	404
240		PRINT 178, QOFF		CONLIM	405
		PRINT 180, NVOL,ITOTAL		CONLIM	406
		PRINT 182		CONLIM	407
		PRINT 184, (I,PHAT(I), I=1,NCOM)		CONLIM	408
		PRINT 250, ID(IFREEZ)		CONLIM	409
250		FORMAT (/43X,44HRESULTS SHOWN ABOVE WERE OBTAINED BY HOLDING/43X,		CONLIM	410
		110HCOMPONENT ,I2,42H FIXED AS THE SLACK COMPONENT VIA OPTION 6//)		CONLIM	411
		PRINT 139		CONLIM	412
		CALL FIT(NCOM,ALPHA,QOFF,NFMIN,NFMAX,IVS,IVCOLS,IERR)		CONLIM	413
		IF (IFREEZ.EQ.0) GO TO 110		CONLIM	414
		GO TO 150		CONLIM	415
C				CONLIM	416
C		COMPLETED ONE SET OF DATA		CONLIM	417
C				CONLIM	418
300		PRINT 320, TITLE		CONLIM	419
320		FORMAT (1H1//20X,17HEND OF ANALYSIS -,8A10)		CONLIM	420
		READ (5,30) OPT		CONLIM	421
		IF (EOF(5)) 340,35		CONLIM	422
340		CALL EXIT		CONLIM	423
		END		CONLIM	424

	SUBROUTINE PSI(NCOMD,NVOL,NFMIN,NFMAX,NFMINX,NFMAXX,IVSIZE,IVCOL,	CONCLIM	425
	1 IERR)	CONCLIM	426
C		CONCLIM	427
C	CONSTRUCTION OF THE INDEX SET PSI BY USE OF HYPERVOLUMES	CONCLIM	428
C		CONCLIM	429
	INTEGER OPT	CONCLIM	430
	DIMENSION N(50),FN(50),FNX(50),PHAT(50),QHAT(50),FN2(50),	CONCLIM	431
	1NSTAR(50),PSAVE(50),OPT(6),JFLAG(5)	CONCLIM	432
	DIMENSION NFMIN(IVCOL,IVSIZE),NFMAX(IVCOL,IVSIZE),	CONCLIM	433
	1 NFMINX(IVCOL,IVSIZE),NFMAXX(IVCOL,IVSIZE)	CONCLIM	434
	COMMON /QVAR/N,FN,FNX,PHAT,QHAT,IFLAG,IVOL,IVS,QLIM,IVC,OPT,	CONCLIM	435
	1ITOTAL,NSTAR	CONCLIM	436
	COMMON /PSIFLG/IPSIFG	CONCLIM	437
	DATA NFAULT/1000000/	CONCLIM	438
C		CONCLIM	439
	IERR = 0	CONCLIM	440
	IPSIFG = 0	CONCLIM	441
	NCOMP = NCOMD	CONCLIM	442
	IF (OPT(4).EQ.2) GO TO 900	CONCLIM	443
	IFLAG = 0	CONCLIM	444
	IUM = 0	CONCLIM	445
	NWORDS = IVCOL*IVSIZE	CONCLIM	446
	MWORDS = NWORDS	CONCLIM	447
	ITOTAL = 0	CONCLIM	448
C		CONCLIM	449
C	INITIALIZATION OF CRITERION FOR HYPERVOLUME ACCEPTANCE INTO PSI	CONCLIM	450
C		CONCLIM	451
	DO 20 I=1,NCOMP	CONCLIM	452
	FN2(I) = 1.0/(FN(I)+2.0)	CONCLIM	453
	PHAT(I) = (FNX(I)+1.0)*FN2(I)	CONCLIM	454
	PSAVE(I) = PHAT(I)	CONCLIM	455
	20 CONTINUE	CONCLIM	456
	QLIM = QTHETA(PHAT)	CONCLIM	457
C		CONCLIM	458
C	INITIALIZE NSTAR	CONCLIM	459
C		CONCLIM	460
	DO 40 ICOMP=1,NCOMP	CONCLIM	461
	NSTAR(ICOMP) = 0	CONCLIM	462
	40 CONTINUE	CONCLIM	463
	IVOL = 1	CONCLIM	464
	IVCHK = 1	CONCLIM	465
	IECS = 1	CONCLIM	466
C		CONCLIM	467
C	START NEW HYPERVOLUME UPPER LIMITS AT STAR VALUES AND THEN WORK	CONCLIM	468
C	UPWARD TO MAXIMUM	CONCLIM	469
C		CONCLIM	470
	100 DO 120 ICOMP=2,NCOMP	CONCLIM	471
	NFMAX(ICOMP,IVOL) = NSTAR(ICOMP)	CONCLIM	472
	XSTAR = NSTAR(ICOMP) + 1	CONCLIM	473
	PHAT(ICOMP) = XSTAR*FN2(ICOMP)	CONCLIM	474
	120 CONTINUE	CONCLIM	475
C		CONCLIM	476
C	DETERMINE UPPER LIMITS ON EACH DIMENSION	CONCLIM	477
C		CONCLIM	478

DO 180 ICOMP=1, NCOMP	CONLIM	479
IF (NSTAR(ICOMP).EQ.N(ICOMP)) GO TO 180	CONLIM	480
NICOMP = N(ICOMP) + 1	CONLIM	481
ISTRN = NSTAR(ICOMP) + 2	CONLIM	482
DO 140 I=ISTRN, NICOMP	CONLIM	483
IA = I-1	CONLIM	484
A = I	CONLIM	485
PHAT(ICOMP) = A*FN2(ICOMP)	CONLIM	486
IF (QTHETA(PHAT) - QLIM) 140,140,160	CONLIM	487
140 CONTINUE	CONLIM	488
NFMAX(ICOMP, IVOL) = IA	CONLIM	489
GO TO 180	CONLIM	490
160 IF (IA.EQ.0) GO TO 170	CONLIM	491
NFMAX(ICOMP, IVOL) = IA - 1	CONLIM	492
A = IA	CONLIM	493
PHAT(ICOMP) = A*FN2(ICOMP)	CONLIM	494
GO TO 180	CONLIM	495
170 NFMAX(ICOMP, IVOL) = 0	CONLIM	496
180 CONTINUE	CONLIM	497
C	CONLIM	498
C SET UP LOWER LIMITS ON EACH COMPONENT	CONLIM	499
C COMPLETES DEFINITION OF A HYPERVOLUME	CONLIM	500
C	CONLIM	501
DO 200 ICOMP=1, NCOMP	CONLIM	502
NFMIN(ICOMP, IVOL) = NSTAR(ICOMP)	CONLIM	503
200 CONTINUE	CONLIM	504
C	CONLIM	505
C CHECK ON OVERLAP AS DETAILED IN ALGORITHM STEP 5	CONLIM	506
C	CONLIM	507
IF (IVCHK.EQ.1) GO TO 430	CONLIM	508
IECI = 1	CONLIM	509
MFLAG = 0	CONLIM	510
IF (IVOL.EQ.1) GO TO 402	CONLIM	511
IEND = IVOL - 1	CONLIM	512
DO 400 ITRY=1, IEND	CONLIM	513
ICHK = IEND - ITRY + 1	CONLIM	514
JF = 0	CONLIM	515
JCOMP = 0	CONLIM	516
DO 300 ICOMP=2, NCOMP	CONLIM	517
IF (NFMAX(ICOMP, IVOL) - NFMIN(ICOMP, ICHK)) 400,210,210	CONLIM	518
210 IF (NFMAX(ICOMP, IVOL) - NFMAX(ICOMP, ICHK)) 240,240,220	CONLIM	519
220 IF (NFMIN(ICOMP, IVOL) - NFMAX(ICOMP, ICHK)) 260,260,400	CONLIM	520
240 IF (NFMIN(ICOMP, IVOL) - NFMIN(ICOMP, ICHK)) 250,300,300	CONLIM	521
250 JCOMP = ICOMP	CONLIM	522
GO TO 300	CONLIM	523
260 IF (JF.EQ.5) GO TO 300	CONLIM	524
JF = JF+1	CONLIM	525
JFLAG(JF) = ICOMP	CONLIM	526
300 CONTINUE	CONLIM	527
C	CONLIM	528
C SCANNED ALL DIMENSIONS IN THE VOLUME	CONLIM	529
C IF OVERLAP EXISTS, USE THEOREMS 2 AND 3 TO SEPARATE VOLUMES.	CONLIM	530
C	CONLIM	531
IF (JCOMP.GT.0) GO TO 340	CONLIM	532



IF (NFMAX(1,IVOL) - NFMAX(1,ICLK)) 302,302,304	CONLIM	533
302 IF (JF.EQ.0) GO TO 500	CONLIM	534
GO TO 305	CONLIM	535
304 IF (JF.EQ.5) GO TO 305	CONLIM	536
JF = JF+1	CONLIM	537
JFLAG(JF) = 1	CONLIM	538
305 DO 310 JI =1,JF	CONLIM	539
JFLG = JFLAG(JI)	CONLIM	540
IF (NFMAX(JFLG,ICLK).LT.N(JFLG)) GO TO 315	CONLIM	541
310 CONTINUE	CONLIM	542
GO TO 500	CONLIM	543
315 NFMIN(JFLG,IVOL) = NFMAX(JFLG,ICLK) + 1	CONLIM	544
LAP = ICHK + IFLAG*IVSIZE	CONLIM	545
IERR = 1	CONLIM	546
GO TO 400	CONLIM	547
340 NFMAX(JCOMP,IVOL) = NFMIN(JCOMP,ICLK) - 1	CONLIM	548
400 CONTINUE	CONLIM	549
402 IF (MFLAG.EQ.IFLAG) GO TO 430	CONLIM	550
CALL READEC(NFMINX,IECI,MWORDS)	CONLIM	551
IECI = IECI + MWORDS	CONLIM	552
CALL READEC(NFMAXX,IECI,MWORDS)	CONLIM	553
IECI = IECI + MWORDS	CONLIM	554
MFLAG = MFLAG + 1	CONLIM	555
DO 420 ITRY=1,IVSIZE	CONLIM	556
ICLK = IVSIZE - ITRY + 1	CONLIM	557
JF = 0	CONLIM	558
JCOMP = 0	CONLIM	559
DO 415 ICOMP=2,NCOMP	CONLIM	560
IF (NFMAX(ICOMP,IVOL) - NFMINX(ICOMP,ICLK)) 420,405,405	CONLIM	561
405 IF (NFMAX(ICOMP,IVOL) - NFMAXX(ICOMP,ICLK)) 408,408,407	CONLIM	562
407 IF (NFMIN(ICOMP,IVOL) - NFMAXX(ICOMP,ICLK)) 414,414,420	CONLIM	563
408 IF (NFMIN(ICOMP,IVOL) - NFMINX(ICOMP,ICLK)) 410,415,415	CONLIM	564
410 JCOMP = ICOMP	CONLIM	565
GO TO 415	CONLIM	566
414 IF (JF.EQ.5) GO TO 415	CONLIM	567
JF = JF + 1	CONLIM	568
JFLAG(JF) = ICOMP	CONLIM	569
415 CONTINUE	CONLIM	570
IF (JCOMP.GT.0) GO TO 419	CONLIM	571
IF (NFMAX(1,IVOL) - NFMAXX(1,ICLK)) 416,416,417	CONLIM	572
416 IF (JF.EQ.0) GO TO 500	CONLIM	573
GO TO 418	CONLIM	574
417 IF (JF.EQ.5) GO TO 418	CONLIM	575
JF = JF + 1	CONLIM	576
JFLAG(JF) = 1	CONLIM	577
418 DO 4180 JI=1,JF	CONLIM	578
JFLG = JFLAG(JI)	CONLIM	579
IF (NFMAXX(JFLG,ICLK).LT.N(JFLG)) GO TO 4190	CONLIM	580
4180 CONTINUE	CONLIM	581
GO TO 500	CONLIM	582
4190 NFMIN(JFLG,IVOL) = NFMAXX(JFLG,ICLK) + 1	CONLIM	583
LAP = ICHK + (MFLAG-1)*IVSIZE	CONLIM	584
IERR = 1	CONLIM	585
GO TO 420	CONLIM	586

419	NFMAX(JCOMP,IVOL) = NFMINX(JCOMP,ICLK) - 1	CONLIM	587
420	CONTINUE	CONLIM	588
	GO TO 402	CONLIM	589
C		CONLIM	590
C	LATEST HYPERVOLUME PROPERLY DESCRIBED - DETERMINE NEXT STARRED	CONLIM	591
C	VALUE IN THE SECOND DIMENSION	CONLIM	592
C		CONLIM	593
430	NSTAR(2) = NFMAX(2,IVOL) + 1	CONLIM	594
	ITUPLE = 1	CONLIM	595
	DO 440 I=1,NCOMP	CONLIM	596
	ITUPLE = ITUPLE*(NFMAX(I,IVOL)-NFMIN(I,IVOL)+1)	CONLIM	597
440	CONTINUE	CONLIM	598
	ITOTAL = ITOTAL + ITUPLE	CONLIM	599
	IVCHK = IVCHK + 1	CONLIM	600
	IF (IVOL.LT.IVSIZE) GO TO 460	CONLIM	601
	CALL WRITEC(NFMIN,IECS,NWORDS)	CONLIM	602
	IECS = IECS + NWORDS	CONLIM	603
	CALL WRITEC(NFMAX,IECS,NWORDS)	CONLIM	604
	IFLAG = IFLAG + 1	CONLIM	605
	IECS = IECS + NWORDS	CONLIM	606
	IVOL = 1	CONLIM	607
	GO TO 600	CONLIM	608
460	IVOL = IVOL + 1	CONLIM	609
	GO TO 600	CONLIM	610
C		CONLIM	611
C	HYPERVOLUME DID NOT CONTRIBUTE - REDUNDANT WITH VOLUMES	CONLIM	612
C	PREVIOUSLY DEFINED	CONLIM	613
C		CONLIM	614
500	NSTAR(2) = MAX0(NSTAR(2),NFMAX(2,IVOL)) + 1	CONLIM	615
C		CONLIM	616
C	STEPS 7 THRU 11 - CALCULATE ALL NEW STARRED VALUES FOR EACH OF	CONLIM	617
C	THE DIMENSIONS - WHEN FOUND, GO BACK THROUGH ENTIRE VOLUME	CONLIM	618
C	DETERMINATION AND CHECKING	CONLIM	619
C		CONLIM	620
600	DO 620 I=1,NCOMP	CONLIM	621
	XSTAR = NSTAR(I) + 1	CONLIM	622
	PHAT(I) = XSTAR*FN2(I)	CONLIM	623
620	CONTINUE	CONLIM	624
	ICOMP = 2	CONLIM	625
	IF (NSTAR(2).GT.N(2)) GO TO 700	CONLIM	626
640	XSTAR = NSTAR(ICOMP) + 1	CONLIM	627
	PHAT(ICOMP) = XSTAR*FN2(ICOMP)	CONLIM	628
C		CONLIM	629
C	SEE IF READY TO GO FIND A NEW HYPERVOLUME	CONLIM	630
C		CONLIM	631
	IF (QTHETA(PHAT) - QLIM) 100,100,700	CONLIM	632
C		CONLIM	633
C	STARRED VALUES REPRESENT CURRENT MINIMUMS - VALUE THAT MUST BE	CONLIM	634
C	USED IN THIS DIMENSION, BY DEFAULT, IS ZERO	CONLIM	635
C		CONLIM	636
700	NSTAR(ICOMP) = 0	CONLIM	637
	PHAT(ICOMP) = FN2(ICOMP)	CONLIM	638
	ICOMP = ICOMP + 1	CONLIM	639
	IF (ICOMP.GT.NCOMP) GO TO 800	CONLIM	640

C		CONLIM	641
C	SET UP THE VALUE FOR THE NEWEST STARRED DIMENSION - USE THE	CONLIM	642
C	MINIMUM OF THE UPPER BOUNDS THAT ARE .GE. THE CURRENT STARRED	CONLIM	643
C	VALUE IN THIS DIMENSION. THAT IS, NEW L* = MIN( U(K,J).GE. L* ).	CONLIM	644
C	NOTE THAT IF U(K,J) = L*, THIS IS THE DEFINED MINIMUM.	CONLIM	645
C		CONLIM	646
	NEXT = NFAULT	CONLIM	647
	IF (IVCHK.EQ.1) GO TO 760	CONLIM	648
	IF (IVOL.EQ.1) GO TO 749	CONLIM	649
	IEND = IVOL-1	CONLIM	650
	DO 750 ITRY =1,IEND	CONLIM	651
	ICHK = IEND - ITRY + 1	CONLIM	652
	IF (NFMAXX(ICOMP,ICHK) - NSTAR(ICOMP)) 750,760,740	CONLIM	653
740	NEXT = MIND(NEXT,NFMAXX(ICOMP,ICHK))	CONLIM	654
750	CONTINUE	CONLIM	655
749	IECI = 1	CONLIM	656
	MFLAG = 0	CONLIM	657
751	IF (MFLAG.EQ.IFLAG) GO TO 758	CONLIM	658
	CALL READEC(NFMINX,IECI,MWORDS)	CONLIM	659
	IECI = IECI + MWORDS	CONLIM	660
	CALL READEC(NFMAXX,IECI,MWORDS)	CONLIM	661
	IECI = IECI + MWORDS	CONLIM	662
	MFLAG = MFLAG +1	CONLIM	663
	DO 756 ITRY=1,IVSIZE	CONLIM	664
	ICHK = IVSIZE - ITRY + 1	CONLIM	665
	IF (NFMAXX(ICOMP,ICHK) - NSTAR(ICOMP)) 756,760,754	CONLIM	666
754	NEXT = MIND(NEXT,NFMAXX(ICOMP,ICHK))	CONLIM	667
756	CONTINUE	CONLIM	668
	GO TO 751	CONLIM	669
C		CONLIM	670
C	NOTE - SINCE L* INDICATES THE MINIMUM FOR THE PREVIOUS SET,	CONLIM	671
C	THERE MUST BE AT LEAST ONE U(K,J).GE.L* PROVIDED THERE	CONLIM	672
C	EXISTS MORE THAN ONE HYPERVOLUME	CONLIM	673
C		CONLIM	674
758	IF (NEXT.EQ.NFAULT) GO TO 760	CONLIM	675
C		CONLIM	676
C	MINIMUM READY FOR THIS DIMENSION	CONLIM	677
C		CONLIM	678
	NSTAR(ICOMP) = NEXT + 1	CONLIM	679
	GO TO 780	CONLIM	680
760	NSTAR(ICOMP) = NSTAR(ICOMP) + 1	CONLIM	681
780	IF (NSTAR(ICOMP).GT.N(ICOMP)) GO TO 700	CONLIM	682
	GO TO 640	CONLIM	683
		CONLIM	684
C		CONLIM	685
C	FINI - ALL HYPERVOLUMES DESCRIBED	CONLIM	686
C		CONLIM	687
800	NVOL = IVCHK-1	CONLIM	688
	IVOL = IVOL-1	CONLIM	689
	IPSIFG = 1	CONLIM	690
	IF (IFLAG.EQ.0) GO TO 900	CONLIM	691
	IF (IVOL.EQ.0) GO TO 900	CONLIM	692
	NWORDS = IVCOL*IVOL	CONLIM	693
	CALL WRITEC(NFMIN,IECS,NWORDS)	CONLIM	694
	IECS = IECS + NWORDS	CONLIM	694

	CALL WRITEC(NFMAX,IECS,NWORDS)	CONLIM	695
C		CONLIM	696
C	CHECK OPTIONS - SEE IF HYPERVOLUME PRINTOUT DESIRED	CONLIM	697
		CONLIM	698
	900 IF (IFLAG.GT.0) GO TO 1000	CONLIM	699
	IF (OPT(3).EQ.0) RETURN	CONLIM	700
	PRINT 905	CONLIM	701
	905 FORMAT (1H1///45X,42H HYPERVOLUME STRUCTURE WITHIN INDEX SET PSI//)	CONLIM	702
	PRINT 910, NVOL,ITOTAL	CONLIM	703
	910 FORMAT (45X,38H NUMBER OF HYPERVOLUMES IN INDEX SET = ,I5/	CONLIM	704
	147X,33H TOTAL NUMBER OF NTUPLES IN SET = ,I6//)	CONLIM	705
	DO 980 I=1,NVOL	CONLIM	706
	PRINT 920, I	CONLIM	707
	920 FORMAT (/20X,10H***VOLUME ,I4/)	CONLIM	708
	DO 960 J=1,NCOMP	CONLIM	709
	PRINT 940, J,NFMIN(J,I),NFMAX(J,I)	CONLIM	710
	940 FORMAT (30X,4HJ = ,I3,2X,9HMIN(J) = ,I4,2X,9HMAX(J) = ,I4)	CONLIM	711
	960 CONTINUE	CONLIM	712
	980 CONTINUE	CONLIM	713
	RETURN	CONLIM	714
	1000 NWORDS = IVCOL*IVSIZE	CONLIM	715
	IECS = 1	CONLIM	716
	KVOL = 0	CONLIM	717
	IF (OPT(3).EQ.0) RETURN	CONLIM	718
	PRINT 905	CONLIM	719
	PRINT 910, NVOL,ITOTAL	CONLIM	720
	DO 1060 I=1,IFLAG	CONLIM	721
	CALL READEC(NFMIN,IECS,NWORDS)	CONLIM	722
	IECS = IECS + NWORDS	CONLIM	723
	CALL READEC(NFMAX,IECS,NWORDS)	CONLIM	724
	IECS = IECS + NWORDS	CONLIM	725
	DO 1040 J=1,IVSIZE	CONLIM	726
	KVOL = KVOL + 1	CONLIM	727
	PRINT 920, KVOL	CONLIM	728
	DO 1020 ICOMP=1,NCOMP	CONLIM	729
	PRINT 940, ICOMP,NFMIN(ICOMP,J),NFMAX(ICOMP,J)	CONLIM	730
	1020 CONTINUE	CONLIM	731
	1040 CONTINUE	CONLIM	732
	1060 CONTINUE	CONLIM	733
	IF (IVOL.EQ.0) RETURN	CONLIM	734
	NWORDS = IVCOL*IVOL	CONLIM	735
	CALL READEC(NFMIN,IECS,NWORDS)	CONLIM	736
	IECS = IECS + NWORDS	CONLIM	737
	CALL READEC(NFMAX,IECS,NWORDS)	CONLIM	738
	DO 1100 J=1,IVOL	CONLIM	739
	KVOL = KVOL + 1	CONLIM	740
	PRINT 920, KVOL	CONLIM	741
	DO 1080 ICOMP=1,NCOMP	CONLIM	742
	PRINT 940, ICOMP,NFMIN(ICOMP,J),NFMAX(ICOMP,J)	CONLIM	743
	1080 CONTINUE	CONLIM	744
	1100 CONTINUE	CONLIM	745
	RETURN	CONLIM	746
	END	CONLIM	747

C	SUBROUTINE COMPAQ(NCOMD,NFMIN,NFMAX,IVSIZE,IVCOL)	CONCLIM	748
C	CROSSCHECK ON HYPERVOLUMES TO INSURE THE MINIMUM AND MAXIMUM	CONCLIM	749
C	LIMITS ON VOLUMES SATISFY BOUND CRITERIA DESCRIBING PSI	CONCLIM	750
C		CONCLIM	751
	DIMENSION N(50),FN(50),FNX(50),PHAT(50),QHAT(50),FN2(50)	CONCLIM	752
	DIMENSION NFMIN(IVCOL,IVSIZE),NFMAX(IVCOL,IVSIZE)	CONCLIM	753
	COMMON /QVAR/N,FN,FNX,PHAT,QHAT,IFLAG,NVOL,IVS,QDMM,IVC	CONCLIM	754
C		CONCLIM	755
	IERR = 0	CONCLIM	756
	IERR1 = 0	CONCLIM	757
	IERR2 = 0	CONCLIM	758
	NCOMP = NCOMD	CONCLIM	759
	PRINT 10	CONCLIM	760
10	FORMAT (1H1//39X,47HCOMPARISON CHECKS ON Q VALUES FOR MINMAX LIMIT	CONCLIM	761
	1S//)	CONCLIM	762
	DO 20 I=1,NCOMP	CONCLIM	763
	FN2(I) = 1.0/(FN(I)+2.0)	CONCLIM	764
	PHAT(I) = (FNX(I)+1.0)*FN2(I)	CONCLIM	765
20	CONTINUE	CONCLIM	766
	QLIM = QTHETA(PHAT)	CONCLIM	767
	PRINT 15, QLIM	CONCLIM	768
15	FORMAT (30X,44HQ VALUE USED FOR INDEX SET CRITERIA, QLIM = ,	CONCLIM	769
	1E20.12//21X,4HKVOL,12X,4HQMIN,14X,9HQLIM-QMIN,13X,4HQMAX,14X,	CONCLIM	770
	29HQLIM-QMAX//)	CONCLIM	771
	KVOL = 0	CONCLIM	772
	MFLAG = 0	CONCLIM	773
	IECI = 1	CONCLIM	774
	NWORDS = IVCOL*IVSIZE	CONCLIM	775
30	IF (MFLAG.EQ.IFLAG) GO TO 50	CONCLIM	776
	IVEND = IVSIZE	CONCLIM	777
40	CALL READEC(NFMIN,IECI,NWORDS)	CONCLIM	778
	IECI = IECI + NWORDS	CONCLIM	779
	CALL READEC(NFMAX,IECI,NWORDS)	CONCLIM	780
	IECI = IECI + NWORDS	CONCLIM	781
	MFLAG = MFLAG + 1	CONCLIM	782
	GO TO 60	CONCLIM	783
50	IF (NVOL.EQ.0) RETURN	CONCLIM	784
	IVEND = NVOL	CONCLIM	785
	IF (IFLAG.EQ.0) GO TO 60	CONCLIM	786
	NWORDS = IVCOL*NVOL	CONCLIM	787
	GO TO 40	CONCLIM	788
60	DO 100 IVOL=1,IVEND	CONCLIM	789
	KVOL = KVOL + 1	CONCLIM	790
	DO 70 I=1,NCOMP	CONCLIM	791
	IF (NFMIN(I,IVOL).GT.N(I)) IERR1 = 1	CONCLIM	792
	AP1 = NFMIN(I,IVOL) + 1	CONCLIM	793
	PHAT(I) = AP1*FN2(I)	CONCLIM	794
70	CONTINUE	CONCLIM	795
	QMIN = QTHETA(PHAT)	CONCLIM	796
	QMIN = QLIM - QMIN	CONCLIM	797
	IF (QMIN.GE. 0.0) GO TO 75	CONCLIM	798
	IERR = 1	CONCLIM	799
	IVR = KVOL	CONCLIM	800
		CONCLIM	801

75 DO 80 I=1,NCOMP	CONLIM	802
IF (NFMAX(I,IVOL).GT.N(I)) IERR1 = 1	CONLIM	803
AP1 = NFMAX(I,IVOL) + 1	CONLIM	804
PHAT(I) = AP1*FN2(I)	CONLIM	805
80 CONTINUE	CONLIM	806
QMAX = QTHETA(PHAT)	CONLIM	807
DMAX = QLIM - QMAX	CONLIM	808
IF (DMAX.GE. 0.0) GO TO 85	CONLIM	809
IERR = 1	CONLIM	810
IVR = KVOL	CONLIM	811
85 PRINT 90, KVOL,QMIN,DMIN,QMAX,DMAX	CONLIM	812
90 FORMAT (20X,I4,5X,E20.12,5X,E10.3,5X,E20.12,5X,E10.3)	CONLIM	813
IF (IERR1.EQ.0) GO TO 100	CONLIM	814
PRINT 92	CONLIM	815
92 FORMAT (15X,10H*****)	CONLIM	816
DO 96 I=1,NCOMP	CONLIM	817
PRINT 94, I,NFMIN(I,IVOL),NFMAX(I,IVOL)	CONLIM	818
94 FORMAT (20X,4HI = ,I2,5X,6HMIN = ,I4,5X,6HMAX = ,I4)	CONLIM	819
96 CONTINUE	CONLIM	820
IERR1 = 0	CONLIM	821
IERRT = IERRT + 1	CONLIM	822
PRINT 92	CONLIM	823
100 CONTINUE	CONLIM	824
IF (IFLAG.EQ.0) GO TO 110	CONLIM	825
IF (IVEND.LT.IVSIZE) GO TO 110	CONLIM	826
GO TO 30	CONLIM	827
110 IF (IERR.EQ.1 .OR. IERRT.GT.0) GO TO 130	CONLIM	828
PRINT 120	CONLIM	829
120 FORMAT (//30X,36HHYPERVOLUME CHECK INDICATES GOOD SET)	CONLIM	830
RETURN	CONLIM	831
130 PRINT 140, IVR	CONLIM	832
140 FORMAT (//20X,40HHYPERVOLUME CHECK INDICATES THAT VOLUME ,I4,23H	CONLIM	833
1IMPROPERLY CONSTRUCTED)	CONLIM	834
RETURN	CONLIM	835
END	CONLIM	836

C	SUBROUTINE FIT(NCOMD,ALPHA,QGFP,NFMIN,NFMAX,IVSIZE,IVCOL,IERR)	CONLIM	837
C		CONLIM	838
C	ROUTINE MATCHES THE Q CURVES ALONG THE H CURVE SO THAT THE	CONLIM	839
C	MAXIMUM Q VALUE CAN BE OBTAINED SATISFYING THE ALPHA-UPPER	CONLIM	840
C	CONFIDENCE LIMIT.	CONLIM	841
C		CONLIM	842
C		CONLIM	843
C	DELTA SHIFT VALUES ARE WEIGHTED ACCORDING TO COMPONENT POSITION	CONLIM	844
C	NTYPE = 0 , SERIES CONNECTION (DELSER)	CONLIM	845
C	= 1 , PARALLEL CONNECTION (DELPAR = SQRT(DELSER) )	CONLIM	846
C		CONLIM	847
C	INTEGER OPT	CONLIM	848
C	DIMENSION N(50),FN(50),FNX(50),PHAT(50),QHAT(50),FACT(50),	CONLIM	849
C	1PSAVE(50),DELH(50),NTYPE(50),PORIG(50),QORIG(50),QM(50),OPT(6),	CONLIM	850
C	2PTIL(50),PLAST(50),ID(10),PFRZ(50),VAL(11),SAVAL(10),IDINV(10)	CONLIM	851
C	DIMENSION NFMIN(IVCOL,IVSIZE),NFMAX(IVCOL,IVSIZE)	CONLIM	852
C	COMMON /QVAR/N,FN,FNX,PHAT,QHAT,IFLAG,NVOL,IVS,QP,IVC,OPT	CONLIM	853
C	COMMON /FACTOR/ FACT	CONLIM	854
C	COMMON /TYPE/NTYPE	CONLIM	855
C	COMMON /FIRST/ IFIRST,DELSER,IFREEZ,NIDS,ID,NLAST,IVAL,VAL,	CONLIM	856
C	1SAVAL,IDINV	CONLIM	857
C	DATA DELMIN/1.0E-06/	CONLIM	858
C		CONLIM	859
C	ONEMAL = 1.0 - ALPHA	CONLIM	860
C	NCOMP = NCOMD	CONLIM	861
C	IERR = 1	CONLIM	862
C	ITHRU = 1	CONLIM	863
C	ITOTM = 0	CONLIM	864
C	NSER = 0	CONLIM	865
C	DO 10 I=1,NCOMP	CONLIM	866
C	IF (NTYPE(I).EQ.1) GO TO 10	CONLIM	867
C	NSER = NSER + 1	CONLIM	868
C	10 CONTINUE	CONLIM	869
C	NSER = MIND(50,10*NSER)	CONLIM	870
C	DELSER = 0.0	CONLIM	871
C	IFIRST = 1	CONLIM	872
C	IF (IFREEZ.GT.0) GO TO 760	CONLIM	873
C	DO 20 I=1,NCOMP	CONLIM	874
C	QHAT(I) = 1.0- PHAT(I)	CONLIM	875
C	PORIG(I) = PHAT(I)	CONLIM	876
C	QORIG(I) = QHAT(I)	CONLIM	877
C	20 CONTINUE	CONLIM	878
C	IF (OPT(1).EQ.0) GO TO 38	CONLIM	879
C	PRINT 25	CONLIM	880
C	25 FORMAT (1H1//)	CONLIM	881
C	PRINT 30, (I,PHAT(I), I=1,NCOMP)	CONLIM	882
C	30 FORMAT (5X,4HI = ,I3,5X,10HPHAT(I) = ,E15.7)	CONLIM	883
C	GO TO 38	CONLIM	884
C	32 ITHRU = 1	CONLIM	885
C	ITOTM = 0	CONLIM	886
C	DELSER = 0.5*DELSER	CONLIM	887
C	DEL2 = 0.5*DELSER	CONLIM	888
C	DELSAV = 0.5*DELSAV	CONLIM	889
C	DELPAR = SQRT(DELSER)	CONLIM	890

DO 35 I=1,NCOMP	CONCLIM	891
PHAT(I) = PORIG(I)	CONCLIM	892
QHAT(I) = QORIG(I)	CONCLIM	893
35 CONTINUE	CONCLIM	894
38 HVALUE = HFUN(NCOMP,NFMIN,NFMAX,IVSIZE,IVCOL)	CONCLIM	895
IF (HVALUE - ONEMAL) 36,37,37	CONCLIM	896
36 ISTAT = -1	CONCLIM	897
GO TO 39	CONCLIM	898
37 ISTAT = 1	CONCLIM	899
39 ISTATC = 1	CONCLIM	900
40 IF (OPT(1).EQ.0) GO TO 45	CONCLIM	901
PRINT 9010, HVALUE	CONCLIM	902
9010 FORMAT (5X,29HHVALUE STARTING OFF DELTAP = ,E15.8)	CONCLIM	903
45 DO 50 I=1,NCOMP	CONCLIM	904
DELH(I) = 0.0	CONCLIM	905
QHAT(I) = 1.0 - PHAT(I)	CONCLIM	906
50 CONTINUE	CONCLIM	907
XNUM = ONEMAL - HVALUE	CONCLIM	908
C	CONCLIM	909
C CHECK VERY FIRST STARTING VALUE TO SEE IF TOO FAR REMOVED	CONCLIM	910
C FROM CURVE FOR ANY CONVERGENCE POSSIBILITY	CONCLIM	911
C	CONCLIM	912
IF (ITHRU.GT.1) GO TO 103	CONCLIM	913
IF (ABS(XNUM) - 0.5*ONEMAL) 100,100,80	CONCLIM	914
80 IF (XNUM) 187,103,189	CONCLIM	915
100 IF (XNUM) 103,103,105	CONCLIM	916
103 IF (ISTAT.EQ.1) GO TO 108	CONCLIM	917
ISTATC = ISTATC + 1	CONCLIM	918
ISTAT = 1	CONCLIM	919
IF (ISTATC .LT. 5) GO TO 108	CONCLIM	920
DELSER = 0.5*DELSER	CONCLIM	921
DELSAV = 0.5*DELSAV	CONCLIM	922
DELPAR = SQRT(DELSER)	CONCLIM	923
ISTATC = 1	CONCLIM	924
GO TO 108	CONCLIM	925
105 IF (ISTAT.EQ.-1) GO TO 110	CONCLIM	926
ISTATC = ISTATC + 1	CONCLIM	927
ISTAT = -1	CONCLIM	928
GO TO 110	CONCLIM	929
108 IF (XNUM) 110,180,110	CONCLIM	930
110 CALL DELTA2(NCOMP,A2,NFMIN,NFMAX,IVSIZE,IVCOL)	CONCLIM	931
DO 120 I=1,NCOMP	CONCLIM	932
PSAVE(I) = PHAT(I)*(1.0 - XNUM/A2)	CONCLIM	933
120 CONTINUE	CONCLIM	934
140 DO 160 I=1,NCOMP	CONCLIM	935
PHAT(I) = PSAVE(I)	CONCLIM	936
QHAT(I) = 1.0 - PSAVE(I)	CONCLIM	937
160 CONTINUE	CONCLIM	938
180 IF (OPT(1).EQ.0) GO TO 185	CONCLIM	939
PRINT 9030, (I,PHAT(I),QHAT(I),I=1,NCOMP)	CONCLIM	940
9030 FORMAT (5X,4HI = ,I2,2X,10HPHAT(I) = ,E15.7,2X,10HQHAT(I) = ,E15.7	CONCLIM	941
1)	CONCLIM	942
185 DO 190 I=1,NCOMP	CONCLIM	943
IF (PHAT(I).LE. 0.0) GO TO 191	CONCLIM	944



IF (PHAT(I).GE. 1.0) GO TO 191	CONCLIM	945
190 CONTINUE	CONCLIM	946
HVALUE = HFUN(NCOMP,NFMIN,NFMAX,IVSIZE,IVCOL)	CONCLIM	947
HSAVE = HVALUE	CONCLIM	948
QP = QTHETA(PSAVE)	CONCLIM	949
ITOTM = ITOTM + 1	CONCLIM	950
IF (ITOTM.GT.NSER) GO TO 1900	CONCLIM	951
QM(ITOTM) = QP	CONCLIM	952
GO TO 1940	CONCLIM	953
C	CONCLIM	954
C LONG PERIOD FOR THIS STEPSIZE - ARE WE PROGRESSING TO MAXIMUM	CONCLIM	955
C	CONCLIM	956
1900 IF ( ABS(QM(NSER)-QM(1)) - DEL2) 530,530,1920	CONCLIM	957
1920 ISTOP = NSER-1	CONCLIM	958
DO 1930 I=1,ISTOP	CONCLIM	959
1930 QM(I) = QM(I+1)	CONCLIM	960
QM(NSER) = QP	CONCLIM	961
1940 IF (OPT(1).EQ.0) GO TO 213	CONCLIM	962
PRINT 9020, HVALUE	CONCLIM	963
9020 FORMAT (5X,28HHVALUE AFTER DELTAP SHIFT = ,E20.12)	CONCLIM	964
PRINT 9040, QP	CONCLIM	965
9040 FORMAT (5X,30HQP VALUE AFTER DELTAP SHIFT = ,E20.12)	CONCLIM	966
GO TO 213	CONCLIM	967
191 IF (ITHRU.GT.1) GO TO 32	CONCLIM	968
IF (XNUM) 187,213,189	CONCLIM	969
C	CONCLIM	970
C STARTING HVALUE TOO FAR REMOVED FROM 1-ALPHA CURVE -	CONCLIM	971
C BISECTION USED TO IMPROVE INITIAL GUESS FOR FIT.	CONCLIM	972
C	CONCLIM	973
187 DO 188 I=1,NCOMP	CONCLIM	974
PLAST(I) = 1.0	CONCLIM	975
188 PHAT(I) = PORIG(I)	CONCLIM	976
ICHKCT = 0	CONCLIM	977
IDIR = 1	CONCLIM	978
GO TO 201	CONCLIM	979
189 DO 192 I=1,NCOMP	CONCLIM	980
PLAST(I) = 0.0	CONCLIM	981
192 PHAT(I) = PORIG(I)	CONCLIM	982
ICHKCT = 0	CONCLIM	983
IDIR = -1	CONCLIM	984
C	CONCLIM	985
C MOVE TOWARD ZERO.	CONCLIM	986
C	CONCLIM	987
193 ICHKCT = ICHKCT + 1	CONCLIM	988
IF (IDIR.EQ.1) GO TO 195	CONCLIM	989
DO 194 I=1,NCOMP	CONCLIM	990
194 PTIL(I) = PHAT(I)	CONCLIM	991
GO TO 197	CONCLIM	992
195 DO 196 I=1,NCOMP	CONCLIM	993
PLAST(I) = PTIL(I)	CONCLIM	994
196 PTIL(I) = PHAT(I)	CONCLIM	995
197 DO 198 I=1,NCOMP	CONCLIM	996
PHAT(I) = PTIL(I) - 0.5*(PTIL(I)-PLAST(I))	CONCLIM	997
198 PHAT(I) = 1.0 - PHAT(I)	CONCLIM	998

	IDIR = -1	CONLIM	999
	GO TO 207	CONLIM	1000
C		CONLIM	1001
	MOVE TOWARD ONE	CONLIM	1002
C		CONLIM	1003
	201 ICHKCT = ICHKCT + 1	CONLIM	1004
	IF (IDIR.EQ.1) GO TO 203	CONLIM	1005
	DO 202 I=1,NCOMP	CONLIM	1006
	PLAST(I) = PTIL(I)	CONLIM	1007
	202 PTIL(I) = PHAT(I)	CONLIM	1008
	GO TO 205	CONLIM	1009
	203 DO 204 I=1,NCOMP	CONLIM	1010
	204 PTIL(I) = PHAT(I)	CONLIM	1011
	205 DO 206 I=1,NCOMP	CONLIM	1012
	PHAT(I) = PTIL(I) + 0.5*(PLAST(I)-PTIL(I))	CONLIM	1013
	206 PHAT(I) = 1.0 - PHAT(I)	CONLIM	1014
	IDIR = 1	CONLIM	1015
	207 IF (OPT(1).EQ.0) GO TO 2070	CONLIM	1016
	DO 9207 I=1,NCOMP	CONLIM	1017
	PRINT 9206, I,PHAT(I)	CONLIM	1018
9206	FORMAT (20X,I2,5X,E15.7)	CONLIM	1019
9207	CONTINUE	CONLIM	1020
2070	DO 208 I=1,NCOMP	CONLIM	1021
	IF (PHAT(I).LE. 0.0) GO TO 201	CONLIM	1022
208	CONTINUE	CONLIM	1023
	DO 209 I=1,NCOMP	CONLIM	1024
	IF (PHAT(I).GE. 1.0) GO TO 193	CONLIM	1025
209	CONTINUE	CONLIM	1026
	HCHECK = HFUN(NCOMP,NFMIN,NFMAX,IVSIZE,IVCOL) - ONEMAL	CONLIM	1027
	IF (OPT(1).EQ.0) GO TO 2090	CONLIM	1028
	PRINT 9210, HCHECK	CONLIM	1029
9210	FORMAT (20X,9HHCHECK = ,E15.7//)	CONLIM	1030
2090	IF (ABS(HCHECK) - 0.5*ONEMAL) 211,211,210	CONLIM	1031
210	IF (HCHECK) 193,211,201	CONLIM	1032
211	IF (OPT(1).EQ.0) GO TO 38	CONLIM	1033
	PRINT 212, ICHKCT	CONLIM	1034
212	FORMAT (10X,I3,36I MOVES WITH BISECTION WERE PERFORMED//)	CONLIM	1035
	GO TO 38	CONLIM	1036
213	IF (1FREEZ.GT.0) GO TO 2110	CONLIM	1037
	CALL SLACK(NCOMP,PHAT,1SLACK)	CONLIM	1038
	IF (1FIRST.EQ.2) GO TO 700	CONLIM	1039
2110	PHATSV = PSAVE(1SLACK)	CONLIM	1040
	IF (OPT(1).EQ.0) GO TO 2130	CONLIM	1041
	PRINT 2120,1SLACK	CONLIM	1042
2120	FORMAT (10X,9HCOMPONENT,I4,28H USED TO MAINTAIN CONSTANT Q)	CONLIM	1043
2130	IREG = NCOMP + 1	CONLIM	1044
	IF (1THRU.GT.1) GO TO 214	CONLIM	1045
	CALL SMDLT(NCOMP,PSAVE,DELSER)	CONLIM	1046
	DEL2 = 0.5*DELSER	CONLIM	1047
	DELSAV = DELSER	CONLIM	1048
	DELPAV = SQRT(DELSER)	CONLIM	1049
	1THRU = 2	CONLIM	1050
	GO TO 215	CONLIM	1051
214	IF (1THRU.EQ.3) GO TO 215	CONLIM	1052

DELSER = DELSAV	CONCLIM	1053
DEL2 = 0.5*DELSER	CONCLIM	1054
DELPAR = SQRT(DELSER)	CONCLIM	1055
215 IF (DELSER - DELMIN) 600,220,220	CONCLIM	1056
220 IREG = IREG - 1	CONCLIM	1057
IF (IREG.EQ.0) GO TO 500	CONCLIM	1058
IF (IREG.EQ.ISLACK) GO TO 220	CONCLIM	1059
IF (NTYPE(IREG).EQ.1) GO TO 225	CONCLIM	1060
DEL = DELSER	CONCLIM	1061
GO TO 228	CONCLIM	1062
225 DEL = DELPAR	CONCLIM	1063
228 PHAT(IREG) = PSAVE(IREG) + DEL	CONCLIM	1064
QHAT(IREG) = 1.0 - PHAT(IREG)	CONCLIM	1065
NEG = 0	CONCLIM	1066
IF (PHAT(IREG).GE. 1.0) GO TO 270	CONCLIM	1067
230 THETA = (QTHETA(PHAT)-PHAT(ISLACK))/QHAT(ISLACK)	CONCLIM	1068
PTRY = (QP - THETA)/(1.0 - THETA)	CONCLIM	1069
IF (PTRY.LE. 0.0) GO TO 260	CONCLIM	1070
IF (PTRY .GE. 1.0) GO TO 260	CONCLIM	1071
PHAT(ISLACK) = PTRY	CONCLIM	1072
QHAT(ISLACK) = 1.0 - PTRY	CONCLIM	1073
H = HFUN(NCOMP,NFMIN,NFMAX,IVSIZE,IVCOL)	CONCLIM	1074
IF (H - HSAVE) 260,400,400	CONCLIM	1075
260 IF (NEG.EQ.1) GO TO 300	CONCLIM	1076
C	CONCLIM	1077
C MAY HAVE MOVED IN WRONG DIRECTION - TRY OTHER WAY	CONCLIM	1078
C	CONCLIM	1079
270 PHAT(IREG) = PSAVE(IREG) - DEL	CONCLIM	1080
QHAT(IREG) = 1.0 - PHAT(IREG)	CONCLIM	1081
NEG = 1	CONCLIM	1082
IF (PHAT(IREG)) 300,300,230	CONCLIM	1083
C	CONCLIM	1084
C CANNOT ACCEPT NEW P(IREG) VALUE - EITHER DEL STEP WAS TOO LARGE	CONCLIM	1085
C TO MAINTAIN A CONSTANT Q VALUE OR H VALUE FOR NEW P(IREG) WAS	CONCLIM	1086
C ON WRONG SIDE OF CURVE (MAINTAIN VALUES OF H .GT. 1-ALPHA).	CONCLIM	1087
C IN EITHER CASE, TRY A SMALLER DEL.	CONCLIM	1088
C	CONCLIM	1089
300 DELH(IREG) = 0.0	CONCLIM	1090
PHAT(IREG) = PSAVE(IREG)	CONCLIM	1091
PHAT(ISLACK) = PHATSV	CONCLIM	1092
QHAT(IREG) = 1.0 - PHAT(IREG)	CONCLIM	1093
QHAT(ISLACK) = 1.0 - PHAT(ISLACK)	CONCLIM	1094
GO TO 220	CONCLIM	1095
C	CONCLIM	1096
C ACCEPTABLE P(IREG) VALUE - MAINTAINED CONSTANT Q AND VALUE OF H	CONCLIM	1097
C ON PROPER SIDE OF CURVE.	CONCLIM	1098
C	CONCLIM	1099
C P VALUES ARE HELD BACK AWAY FROM ABSOLUTE BOUNDARY - WILL ASSUME	CONCLIM	1100
C VALUES VERY CLOSE HOWEVER. PREVENTS H FUNCTION FROM BECOMING	CONCLIM	1101
C INDEFINITE OR INFINITE.	CONCLIM	1102
C	CONCLIM	1103
400 DELH(IREG) = H - HSAVE	CONCLIM	1104
IF (PHAT(IREG) - 1.0) 420,300,300	CONCLIM	1105
420 IF (PHAT(IREG).LE.0.0) GO TO 300	CONCLIM	1106

	HSAVE = H	CONCLIM	1107
	PHATSV = PHAT(ISLACK)	CONCLIM	1108
	GO TO 220	CONCLIM	1109
C		CONCLIM	1110
C	COMPLETED DEL ADJUSTMENT OF ALL P VALUES - NOW DETERMINE WHAT	CONCLIM	1111
C	FURTHER ADJUSTMENTS SHOULD BE MADE.	CONCLIM	1112
C		CONCLIM	1113
	500 IF (OPT(1).EQ.0) GO TO 510	CONCLIM	1114
	PRINT 9060, DELSER	CONCLIM	1115
	9060 FORMAT (5X,18HDEL VALUE TRIED = ,E15.7)	CONCLIM	1116
	PRINT 9030, (I,PHAT(I),QHAT(I),I=1,NCOMP)	CONCLIM	1117
	510 DO 520 I=1,NCOMP	CONCLIM	1118
	IF (DELH(I)) 550,520,550	CONCLIM	1119
	520 CONTINUE	CONCLIM	1120
	530 ITHRU = 3	CONCLIM	1121
	PHAT(ISLACK) = PSAVE(ISLACK)	CONCLIM	1122
	QHAT(ISLACK) = 1.0 - PSAVE(ISLACK)	CONCLIM	1123
	DELSER = 0.5*DELSER	CONCLIM	1124
	DELPAR=SQRT(DELSER)	CONCLIM	1125
	ITOTM = 0	CONCLIM	1126
	DEL2 = 0.5*DELSER	CONCLIM	1127
	IF (DELSER - DELMIN) 600,213,213	CONCLIM	1128
	550 HVALUE = HSAVE	CONCLIM	1129
	GO TO 40	CONCLIM	1130
C		CONCLIM	1131
C	COMPLETED MATCHING OF THE Q AND H CURVES - WE HAVE REACHED THE	CONCLIM	1132
C	MINIMUM DEL SET FOR CONVERGENCE CRITERION	CONCLIM	1133
C		CONCLIM	1134
	600 DO 620 I=1,NCOMP	CONCLIM	1135
	PHAT(I) = PSAVE(I)	CONCLIM	1136
	QHAT(I) = 1.0 - PSAVE(I)	CONCLIM	1137
	620 CONTINUE	CONCLIM	1138
	QOFP = QTHETA(PHAT)	CONCLIM	1139
	IF (PHAT(ISLACK) .LE. (2.0*DELMIN)) IERR = 2	CONCLIM	1140
	RETURN	CONCLIM	1141
C		CONCLIM	1142
C	OSCILLATION IN FIT - CHECK FOR FREEZE OPTION ON COMPONENTS	CONCLIM	1143
C		CONCLIM	1144
	700 IF (OPT(6).NE.0) GO TO 720	CONCLIM	1145
	IFREEZ = NIDS	CONCLIM	1146
	IERR = 3	CONCLIM	1147
	RETURN	CONCLIM	1148
	720 IFREEZ = NIDS	CONCLIM	1149
	DO 740 I=1,NCOMP	CONCLIM	1150
	PFRZ(I) = PSAVE(I)	CONCLIM	1151
	740 CONTINUE	CONCLIM	1152
	HFRZ = HSAVE	CONCLIM	1153
	DELFRZ = DELSER	CONCLIM	1154
	QPFZ = QP	CONCLIM	1155
	ITHUFZ = ITHRU	CONCLIM	1156
	ISLACK = ID(IFREEZ)	CONCLIM	1157
	GO TO 2110	CONCLIM	1158
	760 IFREEZ = IFREEZ-1	CONCLIM	1159
	IF (IFREEZ.EQ.0) RETURN	CONCLIM	1160

```
ISLACK = ID(IFREEZ)
DO 780 I=1,NGCOMP
PSAVE(I) = PFRZ(I)
780 CONTINUE
HSAVE = HFRZ
DELSER = DELFRZ
DELSAV = DELFRZ
QP = QPFRZ
ITHRU = ITHUFZ
GO TO 2110
END
```

```
CONLIM 1161
CONLIM 1162
CONLIM 1163
CONLIM 1164
CONLIM 1165
CONLIM 1166
CONLIM 1167
CONLIM 1168
CONLIM 1169
CONLIM 1170
CONLIM 1171
```

C	SUBROUTINE SLACK(NCOMP,PHAT,ISLACK)	CONLIM	1172
C		CONLIM	1173
C	DETERMINE WHICH SERIES COMPONENT CURRENTLY HAS THE LARGEST PHAT	CONLIM	1174
C	VALUE AND SET ISLACK EQUAL TO THE COMPONENT INDEX FOR USE IN	CONLIM	1175
C	THE FIT ROUTINE. MAINTAIN A SURVEILANCE OVER THE INDICES CHOSEN	CONLIM	1176
C	TO DIAGNOSE CYCLING. TWO CHECKS ARE MADE, THE FIRST TO CATCH	CONLIM	1177
C	REPETITION AND THE SECOND TO DETERMINE IF ACTUAL STEP IMPROVE-	CONLIM	1178
C	MENT IS STILL PROGRESSING OR HALTED.	CONLIM	1179
C		CONLIM	1180
	DIMENSION PHAT(NCOMP), NTYPE(50), ID(10), VAL(11), SAVAL(10), SAVT(10),	CONLIM	1181
	1IDINV(10)	CONLIM	1182
	COMMON /FIRST/ IFIRST, DEL, IFREEZ, N, ID, NLAST, IVAL, VAL, SAVAL, IDINV	CONLIM	1183
	COMMON /TYPE/ NTYPE	CONLIM	1184
C		CONLIM	1185
C	FIND MAXIMUM COMPONENT (SERIES ONLY)	CONLIM	1186
C		CONLIM	1187
	PMAX = 0.0	CONLIM	1188
	DO 20 I=1, NCOMP	CONLIM	1189
	IF (NTYPE(I) .EQ. 1) GO TO 20	CONLIM	1190
	IF (PHAT(I) .LT. PMAX) GO TO 20	CONLIM	1191
	ISLACK = I	CONLIM	1192
	PMAX = PHAT(I)	CONLIM	1193
20	CONTINUE	CONLIM	1194
	IF (IFIRST.EQ.1) GO TO 400	CONLIM	1195
C		CONLIM	1196
C	BEGIN PRIMARY CYCLE CHECK	CONLIM	1197
C		CONLIM	1198
	IF (ISLACK.NE.IDINV(NLAST)) GO TO 100	CONLIM	1199
	IF (N.EQ.1) GO TO 400	CONLIM	1200
	IDEX = N-NLAST+1	CONLIM	1201
	SAVAL(IDEX) = PMAX	CONLIM	1202
	IF (NLAST.EQ.N) GO TO 30	CONLIM	1203
	IF (NLAST.NE.1) GO TO 35	CONLIM	1204
	NLAST = N	CONLIM	1205
	GO TO 40	CONLIM	1206
30	IVAL = IVAL+1	CONLIM	1207
	VAL(IVAL) = PMAX	CONLIM	1208
35	NLAST = NLAST-1	CONLIM	1209
40	IFLAG = IFLAG+1	CONLIM	1210
	IF ( (IFLAG/N) .LT.5 ) RETURN	CONLIM	1211
C		CONLIM	1212
C	COMPLETE CYCLE PERIOD ENCOUNTERED - PERFORM SECONDARY CHECK	CONLIM	1213
C	ON PROGRESS IN CONVERGENCE	CONLIM	1214
C		CONLIM	1215
	IVEND = IVAL-1	CONLIM	1216
	DO 50 J=1, IVEND	CONLIM	1217
	IF (ABS(VAL(J+1)-VAL(J)) - 0.5*DEL) 50,50,60	CONLIM	1218
50	CONTINUE	CONLIM	1219
C		CONLIM	1220
C	NO PROGRESS MADE - WARN FIT ROUTINE AND USER	CONLIM	1221
C		CONLIM	1222
	IFIRST = 2	CONLIM	1223
	RETURN	CONLIM	1224
C		CONLIM	1225

C	SOME PROGRESS MADE - KNOCK OFF FIRST CYCLE AND CONTINUE	CONLIM	1226
C	WITHIN THE PERIOD	CONLIM	1227
C		CONLIM	1228
	60 NLAST = N	CONLIM	1229
	IFLAG = IFLAG-N	CONLIM	1230
	IVAL = IVAL-1	CONLIM	1231
	DO 70 I=1,IVAL	CONLIM	1232
	VAL(I) = VAL(I+1)	CONLIM	1233
	70 CONTINUE	CONLIM	1234
	RETURN	CONLIM	1235
C		CONLIM	1236
C	SLACK COMPONENT DID NOT MATCH THE EXPECTED COMPONENT OF THE CYCLE.	CONLIM	1237
C	IF ONLY ONE COMPONENT IN CYCLE THEN WE ARE BUILDING CYCLE	CONLIM	1238
C	AND WE HAVE A NEW COMPONENT.	CONLIM	1239
C	IF MORE THAN ONE COMPONENT THEN WE MAY HAVE INTERRUPTED THE CYCLE	CONLIM	1240
C	AND THE PERIOD, AND A NEW CYCLE WILL BE FORMED.	CONLIM	1241
C		CONLIM	1242
	100 IF (N.EQ.1) GO TO 300	CONLIM	1243
	INew = 0	CONLIM	1244
	NSTOP = N-1	CONLIM	1245
	DO 120 II=1,NSTOP	CONLIM	1246
	I = II	CONLIM	1247
	IF (ISLACK.EQ.ID(I)) GO TO 160	CONLIM	1248
	120 CONTINUE	CONLIM	1249
	IF (ISLACK.EQ.ID(N)) GO TO 400	CONLIM	1250
C		CONLIM	1251
C	ISLACK AN ENTIRELY NEW COMPONENT - NOW CHECK IF FIRST CYCLE	CONLIM	1252
C	STILL BEING FORMED	CONLIM	1253
C		CONLIM	1254
	IF (IVAL.EQ.1) GO TO 300	CONLIM	1255
C		CONLIM	1256
C	NEW COMPONENT FOR NEW CYCLE - INTERRUPTED OSCILLATION -- REFRESH	CONLIM	1257
C		CONLIM	1258
	I = N-NLAST	CONLIM	1259
	NNEW = N+1	CONLIM	1260
	IVAL = 1	CONLIM	1261
	VAL(1) = SAVAL(NNEW-NLAST)	CONLIM	1262
	GO TO 200	CONLIM	1263
C		CONLIM	1264
C	CYCLE COMPONENT OUT OF PHASE - INTERRUPTED OSCILLATION	CONLIM	1265
C	PICK UP NEW CYCLE WITH COMPONENT IMMEDIATELY FOLLOWING MATCH	CONLIM	1266
C		CONLIM	1267
	160 NNEW = (N-I) + (N-NLAST+1)	CONLIM	1268
	IVAL = 1	CONLIM	1269
	VAL(1) = SAVAL(I+1)	CONLIM	1270
	IF (NNEW.LT.N) GO TO 200	CONLIM	1271
C		CONLIM	1272
C	SPLIT IN OLD CYCLE INTERRUPTED IN MIDDLE WITH DUPLICATE	CONLIM	1273
C	COMPONENT IN SAME CYCLE - NO PARTS IN PREVIOUS CYCLE	CONLIM	1274
C		CONLIM	1275
	NNEW = NNEW-N	CONLIM	1276
	IF (NNEW.EQ.1) GO TO 290	CONLIM	1277
	INew = 1	CONLIM	1278
C		CONLIM	1279

C	NEW CYCLE CREATION USING PARTS OF PREVIOUS CYCLES -- NEW	CONLIM	1280
C	REGENERATE BOOKKEEPING	CONLIM	1281
C		CONLIM	1282
	200 DO 220 J=1,N	CONLIM	1283
	JJ = N-J+1	CONLIM	1284
	220 SAVT(J) = SAVAL(JJ)	CONLIM	1285
	IF (INEW.EQ.0) GO TO 230	CONLIM	1286
	JSTOP = NNEW-1	CONLIM	1287
	GO TO 235	CONLIM	1288
	230 JSTOP = N-NLAST	CONLIM	1289
	IF (JSTOP.EQ.0) GO TO 250	CONLIM	1290
C		CONLIM	1291
C	PICK UP COMPONENTS FROM FIRST PART OF INTERRUPTED CYCLE	CONLIM	1292
C		CONLIM	1293
	235 DO 240 J=1,JSTOP	CONLIM	1294
	JNEW = NNEW-J	CONLIM	1295
	JJ = NLAST+J	CONLIM	1296
	ID(JNEW) = IDINV(JJ)	CONLIM	1297
	240 SAVAL(JNEW) = SAVT(JJ)	CONLIM	1298
	IF (INEW.EQ.1) GO TO 290	CONLIM	1299
	GO TO 260	CONLIM	1300
C		CONLIM	1301
C	EVERYTHING FOR NEW CYCLE FROM PREVIOUS COMPLETED CYCLE	CONLIM	1302
C		CONLIM	1303
	250 JNEW = NNEW	CONLIM	1304
C		CONLIM	1305
C	PICK UP REMAINDER OF NEW CYCLE FROM PREVIOUS COMPLETED CYCLE	CONLIM	1306
C		CONLIM	1307
	260 JSTOP = N-1	CONLIM	1308
	DO 280 J=1,JSTOP	CONLIM	1309
	JNEW = JNEW-1	CONLIM	1310
	ID(JNEW) = IDINV(J)	CONLIM	1311
	280 SAVAL(JNEW) = SAVT(J)	CONLIM	1312
	290 N = NNEW	CONLIM	1313
	IFLAG = N	CONLIM	1314
	NLAST = N	CONLIM	1315
	SAVAL(N) = PMAX	CONLIM	1316
	ID(N) = ISLACK	CONLIM	1317
	DO 295 J=1,N	CONLIM	1318
	JJ = N-J+1	CONLIM	1319
	295 IDINV(J) = ID(JJ)	CONLIM	1320
	RETURN	CONLIM	1321
C		CONLIM	1322
C	NEW MEMBER OF CYCLE -- CON	CONLIM	1323
C		CONLIM	1324
	300 N = N+1	CONLIM	1325
	ID(N) = ISLACK	CONLIM	1326
	SAVAL(N) = PMAX	CONLIM	1327
	IFLAG = IFLAG+1	CONLIM	1328
	DO 320 II=1,NLAST	CONLIM	1329
	I = N-II+1	CONLIM	1330
	320 IDINV(I) = IDINV(I-1)	CONLIM	1331
	IDINV(1) = ISLACK	CONLIM	1332
	NLAST = N	CONLIM	1333



```
RETURN
C
C RESET ALL VALUES TO INITIAL - NEW CYCLE OF A NEW PERIOD
C
400 IFIRST = 0
    N = 1
    IFLAG = 1
    NLAST = 1
    ID(1) = ISLACK
    IDINV(1) = ISLACK
    IVAL = 1
    VAL(1) = PMAX
    SAVAL(1) = PMAX
RETURN
END
```

```
CONLIM 1334
CONLIM 1335
CONLIM 1336
CONLIM 1337
CONLIM 1338
CONLIM 1339
CONLIM 1340
CONLIM 1341
CONLIM 1342
CONLIM 1343
CONLIM 1344
CONLIM 1345
CONLIM 1346
CONLIM 1347
CONLIM 1348
```

C	SUBROUTINE SUB(EX,X,Y)	CONLIM	1349
C		CONLIM	1350
C	THIS SUBROUTINE IS CALLED VIA THE CALL TO RECOVR IN THE MAINLINE	CONLIM	1351
C	WHEN A TIME LIMIT OCCURS. INFORMATION AVAILABLE TO THE USER	CONLIM	1352
C	AT THAT TIME IS PRINTED.	CONLIM	1353
		CONLIM	1354
	DIMENSION N(50),FN(50),FNX(50),PHAT(50),QHAT(50)	CONLIM	1355
	COMMON /QVAR/ N,FN,FNX,PHAT,QHAT,IFLAG,IVOL,IVS,QDMM,IVCOL	CONLIM	1356
	COMMON /PSIFLG/ IPSIFG	CONLIM	1357
	ITOT = IFLAG*IVS + IVOL	CONLIM	1358
	PRINT 20, IFLAG,IVOL,ITOT	CONLIM	1359
	20 FORMAT (1H1///10X,21HRUN WAS NOT COMPLETED//10X,8HIFLAG = ,I10,	CONLIM	1360
	15X,7HIVOL = ,I10//10X,57HTOTAL NUMBER OF HYPERVOLUMES SELECTED AT	CONLIM	1361
	2TIME OF ABORT = ,I6)	CONLIM	1362
	IF (IPSIFG.EQ.1) GO TO 30	CONLIM	1363
	PRINT 25	CONLIM	1364
	25 FORMAT (//10X,61HSUBROUTINE PSI HAD NOT COMPLETED HYPERVOLUME SET	CONLIM	1365
	1CONSTRUCTION)	CONLIM	1366
	GO TO 38	CONLIM	1367
	30 PRINT 35	CONLIM	1368
	35 FORMAT (//10X,57HYPERVOLUME SET CONSTRUCTION WAS COMPLETED PRIOR	CONLIM	1369
	1TO ABORT)	CONLIM	1370
	38 PRINT 40, QDMM	CONLIM	1371
	40 FORMAT (///10X,37HVALUE OF SYSTEM Q AT TIME OF ABORT = ,E15.7)	CONLIM	1372
	STOP	CONLIM	1373
	END	CONLIM	1374

	FUNCTION HFUN(NCOMD,NFMIN,NFMAX,IVSIZE,IVCOL)	CONLIM	1375
	DIMENSION N(50),FN(50),FNX(50),PHAT(50),QHAT(50),FACT(50)	CONLIM	1376
	DIMENSION NFMIN(IVCOL,IVSIZE),NFMAX(IVCOL,IVSIZE)	CONLIM	1377
	COMMON /QVAR/N,FN,FNX,PHAT,QHAT,IFLAG,NVOL,IVS,QDMM,IVC	CONLIM	1378
	COMMON / FACTR/ FACT	CONLIM	1379
	DATA CONST/ 8.1061466795328E-02/	CONLIM	1380
C		CONLIM	1381
C	CALCULATE THE ENTIRE H FUNCTION USING HYPERVOLUMES.	CONLIM	1382
C	THE PROBABILITY VALUES P OF THE FUNCTION ARE OBTAINED FROM	CONLIM	1383
C	INCREMENTAL MOVES (SUBROUTINE FIT).	CONLIM	1384
C		CONLIM	1385
	NCOMP = NCOMD	CONLIM	1386
	HFUN = 0.0	CONLIM	1387
	MFLAG = 0	CONLIM	1388
	IECI = 1	CONLIM	1389
	NWORDS = IVCOL*IVSIZE	CONLIM	1390
	5 IF (MFLAG.EQ.IFLAG) GO TO 10	CONLIM	1391
	IVEND = IVSIZE	CONLIM	1392
	8 CALL READEC(NFMIN,IECI,NWORDS)	CONLIM	1393
	IECI = IECI + NWORDS	CONLIM	1394
	CALL READEC(NFMAX,IECI,NWORDS)	CONLIM	1395
	IECI = IECI + NWORDS	CONLIM	1396
	MFLAG = MFLAG + 1	CONLIM	1397
	GO TO 15	CONLIM	1398
	10 IF (NVOL.EQ.0) RETURN	CONLIM	1399
	IVEND = NVOL	CONLIM	1400
	IF (IFLAG.EQ.0) GO TO 15	CONLIM	1401
	NWORDS = IVCOL*NVOL	CONLIM	1402
	GO TO 8	CONLIM	1403
	15 DO 300 IVOL=1,IVEND	CONLIM	1404
	HPROD = 1.0	CONLIM	1405
	DO 200 ICOMP=1,NCOMP	CONLIM	1406
	NI = N(ICOMP)	CONLIM	1407
	HSUM = 0.0	CONLIM	1408
	ISTRM = NFMIN(ICOMP,IVOL) + 1	CONLIM	1409
	IEND = NFMAX(ICOMP,IVOL) + 1	CONLIM	1410
	RECFAC = PHAT(ICOMP)/QHAT(ICOMP)	CONLIM	1411
	ISTRM = ISTRM-1	CONLIM	1412
	DO 100 I=ISTRM,IEND	CONLIM	1413
	IA = I-1	CONLIM	1414
	AI = IA	CONLIM	1415
	IF (IA.EQ.NI) GO TO 80	CONLIM	1416
	IF (IA.EQ.0) GO TO 60	CONLIM	1417
	IF (NI - 50) 20,20,40	CONLIM	1418
		CONLIM	1419
C		CONLIM	1420
C	UTILIZE STORED FACTORIALS	CONLIM	1421
C		CONLIM	1422
	20 NMIA = NI - IA	CONLIM	1423
	H1 = FACT(NI)/(FACT(IA)*FACT(NMIA))	CONLIM	1424
	IF (IA.GT.ISTRM) GO TO 16	CONLIM	1425
	H2 = (PHAT(ICOMP)**IA)*(QHAT(ICOMP)**NMIA)	CONLIM	1426
	GO TO 18	CONLIM	1427
	16 H2 = H2*RECFAC	CONLIM	1428
	18 HF = H1*H2	CONLIM	1428

C	GO TO 90	CONLIM	1429
C	USE STIRLING APPROXIMATION FOR LOGARITHM OF BINOMIAL COEFFICIENT	CONLIM	1430
C		CONLIM	1431
	40 FNI = FN(ICOMP)	CONLIM	1432
	RM1 = FNI - AI + 1	CONLIM	1433
	IF (1A.GT.ISTRM) GO TO 50	CONLIM	1434
	RM = RM1 - 1.0	CONLIM	1435
	XN1 = FNI + 1.0	CONLIM	1436
	R1 = 1.0/(AI+1.0)	CONLIM	1437
	ORM1 = 1.0/RM1	CONLIM	1438
	TN = 12.0*XN1	CONLIM	1439
	H2 = FNI*ALOG(XN1*QHAT(ICOMP)*ORM1)	CONLIM	1440
	HF = H2 + AI*ALOG(RM1*RECFAC*R1)	CONLIM	1441
	H2 = HF + 0.5*ALOG(XN1*R1*ORM1) + CONST	CONLIM	1442
	HF = EXP(H2 + (AI*RM - XN1*XN1)*R1*ORM1/TN)	CONLIM	1443
	GO TO 90	CONLIM	1444
	50 HF = HF*RECFAC*RM1/AI	CONLIM	1445
	GO TO 90	CONLIM	1446
C		CONLIM	1447
C	AI PARAMETER EQUAL ZERO -- PHAT TERM AND B.C. OUT	CONLIM	1448
C		CONLIM	1449
	60 HF = QHAT(ICOMP)**NI	CONLIM	1450
	H2 = HF	CONLIM	1451
	GO TO 90	CONLIM	1452
C		CONLIM	1453
C	AI PARAMETER EQUAL MAXIMUM N(I) -- QHAT TERM AND B.C. OUT	CONLIM	1454
C		CONLIM	1455
	60 HF = PHAT(ICOMP)**IA	CONLIM	1456
	H2 = HF	CONLIM	1457
C		CONLIM	1458
C	ADD VALUE INTO SUM FOR FOR THIS DIMENSION OF VOLUME	CONLIM	1459
C		CONLIM	1460
	90 HSUM = HSUM + HF	CONLIM	1461
	100 CONTINUE	CONLIM	1462
	HPROD = HPROD*HSUM	CONLIM	1463
	200 CONTINUE	CONLIM	1464
C		CONLIM	1465
C	SUM UP CONTRIBUTION FROM ALL VOLUMES	CONLIM	1466
C		CONLIM	1467
	HFUN = HFUN + HPROD	CONLIM	1468
	300 CONTINUE	CONLIM	1469
	IF (IFLAG.EQ.0) RETURN	CONLIM	1470
	IF (IVEND.LT.IVSIZE) RETURN	CONLIM	1471
	GO TO 5	CONLIM	1472
	END	CONLIM	1473
		CONLIM	1474

```
C
C
C
SUBROUTINE SMDDEL(NCOMD,P,DEL)
DETERMINE THE INITIAL STEPSIZE DELTA
DIMENSION P(NCOMD)
NCOM = NCOMD
XNCOM = NCOM
PSUM = 0.0
DO 20 I=1,NCOM
PSUM = PSUM + P(I)
20 CONTINUE
AVE = PSUM/XNCOM
DEL = 0.1*AVE
RETURN
END
```

```
CONLIM 1475
CONLIM 1476
CONLIM 1477
CONLIM 1478
CONLIM 1479
CONLIM 1480
CONLIM 1481
CONLIM 1482
CONLIM 1483
CONLIM 1484
CONLIM 1485
CONLIM 1486
CONLIM 1487
CONLIM 1488
CONLIM 1489
```

C	SUBROUTINE DELTA2(NCOMD,A2,NFMIN,NFMAX,IVSIZE,IVCOL)	CONLIM	1490
C	ADJUSTMENT FACTOR FOR HYPERVOLUME SYSTEM	CONLIM	1491
C	COMPUTE NECESSARY DELTA VALUE TO MOVE TO THE H CURVE FROM THE	CONLIM	1492
C	CURRENT COORDINATES. MOVE TOWARD CORNER (0,0,....,0).	CONLIM	1493
C		CONLIM	1494
C	DIMENSION N(50),FN(50),FNX(50),PHAT(50),QHAT(50),FACT(50),XNP(50)	CONLIM	1495
	DIMENSION NFMIN(IVCOL,IVSIZE),NFMAX(IVCOL,IVSIZE)	CONLIM	1496
	COMMON /QVAR/ N,FN,FNX,PHAT,QHAT,IFLAG,NVOL,IVS,QDMM,IVC	CONLIM	1497
	COMMON /FACTR/ FACT	CONLIM	1498
	DATA CONST/8.1061466795328E-02/	CONLIM	1499
C		CONLIM	1500
	A2 = 0.0	CONLIM	1501
	NCOMP = NCOMD	CONLIM	1502
	DO 20 I=1,NCOMP	CONLIM	1503
	XNP(I) = FN(I)*PHAT(I)	CONLIM	1504
20	CONTINUE	CONLIM	1505
	MFLAG = 0	CONLIM	1506
	IECI = 1	CONLIM	1507
	NWORDS = IVCOL*IVSIZE	CONLIM	1508
5	IF (MFLAG.EQ.0) GO TO 10	CONLIM	1509
	IVEND = IVSIZE	CONLIM	1510
8	CALL READEC(NFMIN,IECI,NWORDS)	CONLIM	1511
	IECI = IECI + NWORDS	CONLIM	1512
	CALL READEC(NFMAX,IECI,NWORDS)	CONLIM	1513
	IECI = IECI + NWORDS	CONLIM	1514
	MFLAG = MFLAG + 1	CONLIM	1515
	GO TO 15	CONLIM	1516
10	IF (NVOL.EQ.0) RETURN	CONLIM	1517
	IVEND = NVOL	CONLIM	1518
	IF (IFLAG.EQ.0) GO TO 15	CONLIM	1519
	NWORDS = IVCOL*NVOL	CONLIM	1520
	GO TO 8	CONLIM	1521
15	DO 500 IVOL=1,IVEND	CONLIM	1522
	ASUM = 0.0	CONLIM	1523
	DO 400 IM=1,NCOMP	CONLIM	1524
	APROD = 1.0	CONLIM	1525
	DO 300 IN=1,NCOMP	CONLIM	1526
	AISUM = 0.0	CONLIM	1527
	NI = N(IN)	CONLIM	1528
	ISTRT = NFMIN(IN,IVOL) + 1	CONLIM	1529
	IEND = NFMAX(IN,IVOL) + 1	CONLIM	1530
	RECFAC = PHAT(IN)/QHAT(IN)	CONLIM	1531
	ISTRM = ISTRT - 1	CONLIM	1532
	DO 200 I= ISTRT,IEND	CONLIM	1533
	IA = I-1	CONLIM	1534
	AI = IA	CONLIM	1535
	IF (IA.EQ.NI) GO TO 100	CONLIM	1536
	IF (IA.EQ.0) GO TO 80	CONLIM	1537
	IF (NI - 50) 40,40,60	CONLIM	1538
C		CONLIM	1539
C	UTILIZE STORED FACTORIALS	CONLIM	1540
C		CONLIM	1541
		CONLIM	1542
		CONLIM	1543

40	NMIA = NI - IA	CONLIM	1544
	H1 = FACT(NI)/(FACT(IA)*FACT(NMIA))	CONLIM	1545
	IF (IA.GT.ISTRM) GO TO 50	CONLIM	1546
	H2 = (PHAT(IN)**IA)*(QHAT(IN)**NMIA)	CONLIM	1547
	GO TO 55	CONLIM	1548
50	H2 = H2*RECFAC	CONLIM	1549
55	HF = H1*H2	CONLIM	1550
	GO TO 120	CONLIM	1551
C		CONLIM	1552
C	USE STIRLING APPROXIMATION FOR LOGARITHM OF BINOMIAL COEFFICIENT	CONLIM	1553
C		CONLIM	1554
60	FNI = FN(IN)	CONLIM	1555
	RM1 = FNI - AI + 1	CONLIM	1556
	IF (IA.GT.ISTRM) GO TO 70	CONLIM	1557
	RM = RM1 - 1.0	CONLIM	1558
	XN1 = FNI + 1.0	CONLIM	1559
	R1 = 1.0/(AI+1.0)	CONLIM	1560
	ORM1 = 1.0/RM1	CONLIM	1561
	TN = 12.0*XN1	CONLIM	1562
	H2 = FNI*ALOG(XN1*QHAT(IN)*ORM1)	CONLIM	1563
	HF = H2 + AI*ALOG(RM1*RECFAC*R1)	CONLIM	1564
	H2 = HF + 0.5*ALOG(XN1*R1*ORM1) + CONST	CONLIM	1565
	HF = EXP(H2 + (AI*RM - XN1*XN1)*R1*ORM1/TN)	CONLIM	1566
	GO TO 120	CONLIM	1567
70	HF = HF*RECFAC*RM1/AI	CONLIM	1568
	GO TO 120	CONLIM	1569
C		CONLIM	1570
C	AI PARAMETER EQUAL ZERO -- PHAT TERM AND B.C. OUT	CONLIM	1571
C		CONLIM	1572
80	HF = QHAT(IN)**NI	CONLIM	1573
	H2 = HF	CONLIM	1574
	GO TO 120	CONLIM	1575
C		CONLIM	1576
C	AI PARAMETER EQUAL MAXIMUM N(I) -- QHAT TERM AND B.C. OUT	CONLIM	1577
C		CONLIM	1578
100	HF =PHAT(IN)**IA	CONLIM	1579
	H2 = HF	CONLIM	1580
C		CONLIM	1581
C	CHECK TO SEE IF WE WANT DELTA(M,N) FACTOR	CONLIM	1582
C		CONLIM	1583
120	IF (IN.NE.IM) GO TO 140	CONLIM	1584
	HF = HF*(XNP(IN) - AI)/QHAT(IN)	CONLIM	1585
140	AISUM = AISUM + HF	CONLIM	1586
200	CONTINUE	CONLIM	1587
	APROD = APROD*AISUM	CONLIM	1588
300	CONTINUE	CONLIM	1589
	ASUM = ASUM + APROD	CONLIM	1590
400	CONTINUE	CONLIM	1591
C		CONLIM	1592
C	SUM UP VALUES FOR ALL VOLUMES	CONLIM	1593
C		CONLIM	1594
	A2 = A2 + ASUM	CONLIM	1595
500	CONTINUE	CONLIM	1596
	IF (IFLAG.EQ.0) RETURN	CONLIM	1597

IF (IVEND.LT.IVSIZE) RETURN  
GO TO 5  
END

CONLIM 1598  
CONLIM 1599  
CONLIM 1600